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# Model for Molten Salt Corrosion of (Co,Cr)-Based Superalloys

Lawrence P. Cook and David W. Bonnell

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National Bureau of Standards  
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**U.S. DEPARTMENT OF COMMERCE, C. William Verity, *Secretary***  
**NATIONAL BUREAU OF STANDARDS, Ernest Ambler, *Director***



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### Abstract

An integrated equilibrium kinetic model is described for treating the chemical solution component of corrosion of (Co,Cr)-based superalloys by the (Na, S, V)-molten salts originating from impurities present in hydrocarbon fuels. Gas phase chemistry and gas phase/condensed phase precipitate interactions are modeled using the NASA-Lewis multicomponent free energy minimization program (CEC). Salt deposition rates are calculated with the aid of a chemical frozen boundary layer (CFBL) program. Solubilities of superalloy components (Co and Cr) are modeled from phase equilibrium data, and rate of solution is described by assuming a very thin steady state oxide film, with formation and dissolution occurring according to a parabolic rate law. A range of steady state corrosion rates can be predicted using this approach which are in general agreement with the range of reported test rig results. Further model development would benefit from additional experimental phase equilibrium data on the system  $\text{Na}_2\text{O}-\text{CoO}-\text{Cr}_2\text{O}_3-\text{SO}_3-\text{V}_2\text{O}_5$ .



## I. BACKGROUND

### A. The Problem of Hot Corrosion

The phenomenon of hot corrosion has received much attention over the past several decades; the state of our knowledge with regard to metals has been summarized in ref. [1]. Much of the most recent interest has centered on hot corrosion of superalloys, in particular, corrosion of superalloys or superalloy with coatings based on Ni, Co, Cr, Al, and Y. In most boiler and gas turbine applications, hot corrosion of these and other materials is due to the chemical action of fuel impurities such as Na, S and V. When these impurities condense out as salts, mass transport of superalloy components occurs which leads to degradation and removal of material from the superalloy surface, and provides a mechanism for oxidative attack on the alloy constituents. While hot corrosion is essentially a chemically driven process, quantitative chemical models describing this process have not been developed.

Two thermal regimes pertaining to hot corrosion have been distinguished by corrosion engineers and materials scientists working in the area of combustion [2]. Low temperature hot corrosion is apparently limited to 650-750 °C. This form of corrosion is characterized by deep smooth pits with sharp boundaries [ref. 3]; the pits are filled with oxides of Al and Cr. Nickel and cobalt are strongly depleted in the oxide relative to the metal. Typically a thin layer of sulfide occurs intermittently along the oxide/metal interface.

High temperature hot corrosion (alternatively referred to as Type 1 corrosion in ref. [2]) occurs near 900 °C (1600 °F) and is characterized by a thick

porous oxide scale, often containing detached metal particles. The metal/oxide interface is highly irregular and deep penetration of the oxide into the metal occurs. A layer of sulfides may occur near the base of the oxide.

#### B. Previous Models

Generalized models have been suggested for the simple oxidation of metals, perhaps the most notable being the diffusional model of Wagner [4], which has been supported by the observation of parabolic rate laws for several systems involving pure metals. Hot corrosion models must necessarily consider additional factors relating to the complex multicomponent chemistry and the gradients prevailing at the interfaces between metal, scale, molten salt and gas. Some of the necessary considerations are summarized in ref. [5]. One type of general hot corrosion model is represented by the fluxing models of Goebel and Pettit [6], Rapp and Goto [7] and others. In these models, oxide scale is dissolved by the salt, transported and reprecipitated at another site (typically the salt/gas interface). An alternative model proposed by Hancock [8] involves scale cracking and salt penetration of the metal.

The effects of certain variables known to influence corrosion rates, such as thermal cycling, are difficult to model. By contrast, the equilibrium solution chemistry can be modeled, if basic thermodynamic or phase equilibrium data are available. As an indication of the promise this approach holds, Jones [9] has outlined a qualitative model for low temperature hot corrosion which relates to the effect of  $P_{SO_3}$  on the removal of cobalt in the form of

molten cobalt/sodium mixed salts. In addition to  $P_{SO_3}$  and the activity of  $Na_2SO_4$ , the activity of  $V_2O_5$  has a well known effect on corrosion rates. This has been treated by the statistical model of Rathnammma and Bonnell [10].

### C. Goals of the Present Study

Given the complexity of available hot corrosion data, it is not surprising that comprehensive chemical models have not been developed. The present study attempts to isolate and estimate the chemical solution component of the corrosion of Co, Cr based alloys by Na, S, V - containing fuels. This will allow an assessment of the importance of the chemical solution contribution to the over-all corrosion rate.

## II. OUTLINE OF MODEL

The model presented here is concerned with the mass transport of the Cr and Co components of the superalloy. A representative commercial superalloy [ref. 11] contains (wt.%): 22% Cr, 71.5% Co, 6% Al and 0.5% Y. Cobalt and chromium are the dominant constituents and effective removal of these components (either mechanically or chemically) must occur for corrosion to be extensive. The Cr component is known to improve corrosion resistance by forming a protective scale. Although present in minor amounts; the Al and Y are also very important; however the manner in which these components improve the corrosion resistance of the superalloy is not fully understood. One suggestion [ref. 12] is that Y and Al serve to make the protective oxide film finer grained (hence less porous) and more adherent. Although the model discussed here is currently limited to consideration of the chemistry of

Co and Cr, it should nonetheless be applicable to the observed corrosion of superalloys.

The present model considers the effects of Na, S and V fuel impurities on corrosion. The essential features of the model treated here are given in Fig. 1, and will be discussed in the following sections of this report.

Briefly, the model consists of the following segments:

1. calculation of combustion and wall equilibria
2. calculation of salt deposition rates
3. calculation of salt phase equilibria and CoO, Cr<sub>2</sub>O<sub>3</sub> solubilities
4. modeling of CoO, Cr<sub>2</sub>O<sub>3</sub> film formation and solution rates
5. estimation of corrosion rates

The model is compared with burner test rig data to give an indication of the utility of the present approach, along with suggestions for follow-up.

### III. CALCULATION OF GAS EQUILIBRIA

#### A. Methodology

As indicated in Fig. 1, the initial requirement for modeling is knowledge of the gas phase chemistry. It is generally possible to calculate the equilibrium species composition of the combustion gases, including the effect of the fuel impurities, if adequate thermodynamic data are available for all significant species. Where precipitation occurs, it is necessary to model the solution process in order to obtain activity data. The most general method currently available for solving the multicomponent equilibrium problem depends on minimizing the Gibbs Energy (G) for the entire system of known possible

species. For systems where many possible species exist, typical of corrosion systems, a variety of computer codes exist which will minimize the Gibbs energy ( $G$ ) of a gas mixture, possibly in contact with a collection of pure independent phases. Only recently [13,14] have techniques been developed for handling condensed solutions with variable stoichiometry. The basic method consists of solving a set of simultaneous equations for the free energy of the system, subject to the constraint of mass balance. The general solution techniques used do not *a priori* restrict the computation to non-negative amounts for individual species or phases. Thus, the problem must be solved iteratively, eliminating phases with negative amounts. Once convergence of the mass balance at minimum  $G$  is obtained, it is then necessary to iterate by selecting alternate phase sets for possible improvement of the free energy minimum, followed each time by iteratively reconverging the mass balance. The process is continued until no alternative phase-set obeying the phase rule can further lower the system free energy.

For the present report, gas/condensed phase equilibrium calculations were completed using a modified version of the NASA-Lewis Research Center multicomponent equilibrium program which is referred to here as the CEC program [15]. The modifications permit the program to properly handle multiple solutions (liquids e.g.) with non-unity component activities. This is particularly important as most of the species expected to be important in hot corrosion are present as trace species in solution, and with the exception of solids, are unlikely to precipitate as pure phases. Although the modified CEC code treats only ideal solutions, Hastie and Bonnell [16] have shown that an ideal solution model can correctly model solutions considered highly

non-ideal when the proper species are included. Although this is yet to be shown true for the CEC database, assuming ideal solution behavior with regard to multicomponent species is an appropriate first step.

Although the modified CEC program is not generally available, and details of the implementation permitting multiple condensed phase mixtures are not available, the general procedure is as described above, and hand checks on a sample run indicate that the various species in solution have the proper thermodynamic equilibrium constant relationships. The program has also been extensively tested at NASA-Lewis. In particular, a number of stability improvements were made particularly for David Taylor Naval Ship R&D Center to permit the program to successfully converge with input specifying one or more atoms of species to be present in parts per million or less concentration.

The modified program uses a similar input structure to that of CEC, using an extensive database of thermodynamic species. The program still selects needed data from that database automatically, relieving the user of the database preparation in simpler cases. The extra mixture(s) beyond the gas phase are specified by including groups of species names, in the familiar INSERT/OMIT format, following an identifier record (eg. SOLN 2) entered right after the REACTANTS records. Although this database formalism, and the method of denoting solution species is relatively much easier for the occasional user, there is a potential problem of some magnitude. The database for CEC represents pure phases, each defined by a polynomial for the Cp function in the temperature region of validity, and heat and entropy terms (see Hastie and Bonnell, [16] for the form of these entries) from which the species Gibbs

energy can be calculated. For a problem where only pure phases are expected, the fact that the database was designed to permit CEC to select the most stable phase at the calculation temperature is desirable. However, in the case of solutions, the modified CEC program continues to substitute the most stable phase, regardless of the fact that it is not appropriate to use; for example, functions for the solid form of a species are used to represent its Gibbs energy in a liquid solution. This problem occurs whenever the liquidus temperature drops below the melting point of constituent species.

Substitution of the solid thermodynamic functions progressively over-stabilizes the solution by the  $\Delta G(T)$  of melting. This problem is not easily remedied, as the data base entries were not originally fit expecting extrapolation beyond the stability regions. Rather, the intent was best representation of the pure phase stability. This problem is general for database-driven equilibrium codes, and is not unique to the modified CEC code. The code should assume extrapolatable functions, and use the most stable phase matching the state (gas, liquid, solid) of the mixture. Since the majority of calculations for this work, were at temperatures near or above the melting point of all solution species, the calculated equilibria should be close to the true values. In any case, since the effect is to accentuate the stability of the liquid solution, any error in a corrosion estimate based on solution solubilities tends to be conservative.

Another difficulty is that when CEC determines that a solution phase is not stable for a chosen temperature, the solution is removed permanently. The code does not further consider it for lower temperature problems. Since CEC convergence is generally much more reliable working from higher temperatures

to lower, this is a significant problem. It makes impossible the simultaneous calculation of the combustion composition and the downstream (wall) equilibria for simple entry to Chemical Frozen Boundary Layer [CFBL] program described in Section IV.

#### B. Input Data

##### i. Fuel and Fuel/Oxidant Ratio

Possible fuel stoichiometries range from  $\text{CH}_{1.5}$  to  $\text{CH}_{2.0}$ . For turbine applications, a value of  $\text{CH}_{1.8}$  is typical; for most boiler applications a value of  $\text{CH}_{2.0}$  may be typical. For purposes of carrying out the model calculations, we have used a value of  $\text{CH}_{1.8}$ ; however the effect of varying fuel composition between  $\text{CH}_{1.8}$  and  $\text{CH}_{2.0}$  on composition of salts would probably be negligible.

Possible fuel oxidant ratios (fuel: air, by volume) range from 1:10 to 1:100. In practice, typical ratios are near 1:30 for boiler operation and 1:50 for turbines. For the present calculations the main effect of varying the fuel/air ratio would be on  $P_{O_2}$ , and on the adiabatic flame temperature. However, for the range of  $P_{O_2}$  considered here (see below), the effect of such variations on salt chemistry would probably be insignificant. For purposes of modeling we have used a fuel/oxidant ratio of 1:30; this is equivalent to a fuel-to-oxidant weight ratio of 0.04538, based on a fuel density of 1.38 g/cm<sup>3</sup>, typical of kerosene-type turbine fuels. The oxidant used in the calculations corresponds to clean air, with one wt. % water vapor present.

### ii. Temperature and Pressure

While flame temperatures may reach 2600 °C during combustion, depending upon heat transfer, fuel/oxidant, preheat, etc., the temperatures of the downstream components subject to hot corrosion range from 600 to 1000 °C. We have selected two temperatures for model calculations: 977 K (1300 °F) and 1177 K (1650 °F). These temperatures approximate the thermal regimes of low temperature and high temperature hot corrosion (~700 and ~900 °C, respectively).

Pressures in operating combustion systems vary widely depending on conditions of mass flow and the system design, but typically turbines operate at pressures above 1 atm. To study the effect of pressure on salt compositions we have completed model calculations at 1, 5, 7, 10, and 15 atm total pressure.

### iii. Concentration of Na, S, V in Fuels

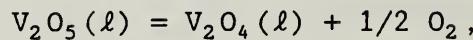
Impurity concentrations currently of interest to the Navy are summarized in Table 1, corresponding to "base" fuel, fuel "GT10", and fuel "GT12". To provide a range of impurity concentrations which encompass the fuels in Table 1, we have completed model calculations using the matrix of impurity concentrations in Table 2. Thus sodium contents range from 0.1 ppm (wt.) to 10 ppm; sulfur from 0.01 to 1.0 wt%, and vanadium from 0.1 to 10 ppm (wt.). The matrix of fuels represented by Table 2 leads to 27 different impurity compositions. For purposes of ease in referring to these compositions we shall use a nomenclature in which the values of (Na, S, V) respectively are indicated according to the row of Table 2 in which they fall. Thus,

composition (111) represents 0.1 ppm Na, 0.01 wt% and 0.1 ppm V; composition (132) represents 0.1 ppm Na, 1.0% S and 1.0 ppm V, etc.

#### iv. Thermodynamic Database

The database installed at NASA-Lewis for use with the modified CEC code consists of the latest NASA thermodynamic database (1986), with the addition of an extensive set of metal vanadates, including solid and some liquid vanadates for Al, Sb, Ba, Bi, Cd, Ca, Ce, Cr, Co, Cu, Hf, In, Fe, La, Li, Pb, Mg, Mn, Mo, Nd, Ni, K, Ag, Na, Sr, Sn, Sn, Ti, W, Y, Zn, and Zr, based on an extensive literature search and considerable estimation by workers at Aerodyne under contract to DTNSR&DC, Annapolis. For the model runs reported here, Table 3 gives the species considered for the compositions modeled. The phase notation for all species is given in parenthesis except for the gas phase species.

The most conspicuous missing species in this data base pertinent to vanadium transport is a gas species of  $V_2O_5$  stoichiometry. A general literature survey has been made by JANAF [17], but their critical assessment of the gas phase data has not provided a clear cut vaporization mechanism. It is likely that the vaporization process is incongruent, with a variety of gas species. Although JANAF [17] calculates a "decomposition temperature" of 1963 K at  $P_{O_2} \approx 1$  atm for the equilibrium,



one or more vanadium oxide species are also major gas species. The literature is quite uncertain regarding the nature of these species, owing to a scarcity

molecular specific (ie. mass spectrometric) studies. It is clear that this system is overdue for careful study, including experiments where the oxygen partial pressure can be controlled to permit measurements in well defined V-O phase regions. The database for CEC supplied to NBS contained the gas species  $\text{VO}$  and  $\text{VO}_2$ , but had no entries for what is considered the majority gas species,  $\text{V}_4\text{O}_{10}$  (dimeric  $\text{V}_2\text{O}_5$ ). Part of the problem is that there are essentially two groups of measurements, represented by the data of Polyakov [18] at high temperature limit, and the data of Semenov, et al [19]. The mass spectrometric results of Farber, et al [20] are more in accord with the Semenov [19] data, but their results suggest rapid conversion to a lower oxide (probably  $\text{V}_2\text{O}_3(s)$ ) with  $\text{V}_4\text{O}_8$  becoming quite important. Fig. 2 shows the relative partial pressures of the various experimental data. CEC calculations performed with the non-solution version using the coefficients of Table 4 indicate that the Polyakov [18] data will cause  $\text{V}_4\text{O}_{10}$  to become the dominant vanadium gas carrier. On the other hand, the Semenov et al [Ref. 19] and Farber et al [20] data indicate that the pressures of  $\text{VO}_2$  and  $\text{V}_4\text{O}_{10}$  are comparable in the temperature regime of interest. For the purposes of this project, it was decided that ignoring  $\text{V}_4\text{O}_{10}$  would be as reasonable as including a possibly erroneous value. It is clear that more experimental on the V-O system is warrented. In particular, a mass spectrometric study where the partial pressure of  $\text{O}_2$  can be controlled is necessary to ascertain the importance of gas species such as  $\text{V}_4\text{O}_8$ . In any case, an early test of the effect of adding  $\text{V}_4\text{O}_{10}$  to the data base is highly recommended, particularly before the vanadate database is used extensively.

### C. Results

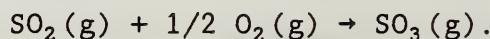
Results of CEC equilibrium calculations for fuels with impurity levels of Table 2 under the conditions outlined above are summarized in tabular form in Appendix A. For corrosion modeling important variables are  $P_{O_2}$ ,  $P_{SO_3}$  and mole fractions of the components  $Na_2SO_4$ ,  $V_2O_5$  and  $Na_2V_2O_6$  in the molten salt phase.

#### i. Oxygen Partial Pressure ( $P_{O_2}$ )

As examination of the data in Appendix A shows, oxygen partial pressure does not vary significantly under the conditions of the calculations and falls in the range 6.3 to  $6.7 \times 10^{-2}$  atm., as would be expected from the large excess of  $O_2$  in the combustion process.  $P_{O_2}$  is not affected appreciably by increasing the total pressure from 1 to 15 atm.

#### ii. Sulfur Trioxide Partial Pressure ( $P_{SO_3}$ )

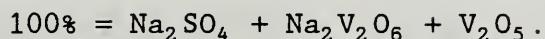
The equilibrium partial pressures of sulfur dioxide, sulfur trioxide and oxygen are related by the reaction:



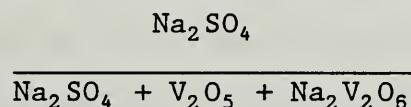
Thus, it is sufficient to specify either  $P_{SO_2}$  or  $P_{SO_3}$  along with  $P_{O_2}$  to define the sulfur activity in the system. Increasing the total pressure increases the ratio of  $P_{SO_3}/P_{SO_2}$ ; increasing the temperature has the opposite effect. Increasing the total pressure from 1 to 10 atm. increases the value of  $P_{SO_3}$  by about threefold at 1172 K and by one-and one-half to two times 977 K. As would be expected, values of  $P_{SO_3}$  vary widely with sulfur content of the fuel, and range from about  $3 \times 10^{-7}$  atm for fuel with 0.01 wt% S to about  $1.5 \times 10^{-4}$  atm for fuel with 1 wt% S.

### iii. Condensed Phase Compositions

The data for the liquid phase in Appendix A have been recalculated to (mole basis):



A plot of the recalculated data is shown in Fig. 3, where it can be seen that essentially the complete range of possible molar ratios is encompassed with regard to these three components. The groupings that occur in Fig. 3 are related to the necessarily limited distribution of fuel impurity ratios considered in Table 2. The labeling in Fig. 3 allows the groupings to be related to Table 2, according to the labeling convention defined above in section III.B.iii. As Fig. 3 contains all the data from Appendix A, the effect of T and P are not clearly delineated. For this reason, Fig. 4 has been included which shows only data for composition (111); it is clear that increasing pressure increases the ratio:

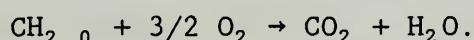


This effect is greatest in increasing from one to two atm. pressure. Increasing the temperature has the opposite effect.

## IV. CALCULATION OF SALT DEPOSITION RATES

### A. Methodology

Gokoglu et al [21] have developed a chemical frozen boundary layer (CFBL) code for calculation of salt deposition rates on the walls of combustion systems. This code has built-in constants for the properties of the system where combustion is complete and dominated by the reaction



The alkali/sulfur species considered in the gas phase (Na system) are: (1) NaOH, (2) Na, (3) Na<sub>2</sub>SO<sub>4</sub>, (4) SO<sub>2</sub>, (5) SO<sub>3</sub>, (6) NaCl, (7) H<sub>2</sub>S. Work by Rathnamma and Nagarajan [22] supports the contention that the deposition rates for other salts (e.g. Na<sub>2</sub>V<sub>2</sub>O<sub>6</sub>, V<sub>2</sub>O<sub>5</sub>) parallel very closely their relative quantities from the equilibrium calculations. Thus, for the purposes of this work, vanadium salt deposition rates were presumed to be in proportion (relative to the calculated Na<sub>2</sub>SO<sub>4</sub> deposition rates) according to their equilibrium concentration in the calculated solution. This is a reasonable working assumption, as the resulting error is less than that due to other modeling assumptions relating to the physical behavior of the wall deposit. Gokoglu and Santoro [23] have recently reported experimental results in excellent agreement with CFBL calculations.

The version of the CFBL code implemented was nearly identical to the version reported by Gokoglu et al [Ref. 21]. In installing the code on the NBS CYBER 855 system, a few instances of attempts to reference undefined variables were encountered. Subsequent examination of the code indicated that zero entries were correct, and thus the code had been performing correctly on its development system, where a reference to undefined storage returns an appropriate zero. The authors were contacted to confirm this. For convenience, and for general use, the corrected version was assembled for use on 8088/8086/80286/80386-based MS-DOS microcomputer systems with floating point coprocessors.

### B. Input Data

The CFBL code requires certain input parameters specifying the area of the deposition surface, size of the gas jet, mass flow, etc. These have been chosen to correspond as closely as possible to burner test rigs for which deposition rate data are available. CFBL input parameters are listed in Appendix B.

### C. Results

Results of a series of CFBL calculations for nine compositions from Table 2 are given in Appendix B. The compositions chosen reflect the impurity compositions with the highest sulfur content (1.0 wt. %). Phase compositions of the deposited salts are shown in Table 5, along with total deposition rates. It is evident that calculated salt deposition rates vary dramatically, depending upon salt composition.

## V. CHEMICAL MIXING

### A. Methodology

For many salt systems a simple regular solution model provides adequate description of the mixing properties [24]. For a ternary system minimum input would be thermodynamic properties of the end members and phase equilibrium information on the binary invariant points. As noted, we are interested, for purposes of this report, in solubilities of CoO and Cr<sub>2</sub>O<sub>3</sub> in mixtures of Na<sub>2</sub>SO<sub>4</sub>-V<sub>2</sub>O<sub>5</sub>-Na<sub>2</sub>VO<sub>6</sub> salts. Unfortunately there are not sufficient phase equilibrium data on the limiting binary systems to develop a realistic regular solution model - therefore we have had to assume that with regard to mixtures of CoO, Cr<sub>2</sub>O<sub>3</sub>, Na<sub>2</sub>SO<sub>4</sub>, Na<sub>2</sub>V<sub>2</sub>O<sub>6</sub> and V<sub>2</sub>O<sub>5</sub>, the heats of mixing are zero. This

same assumption has already been noted concerning the CEC calculation of gas/salt equilibria, and may provide a reasonable approximation, since if the proper mixing species are chosen, the enthalpies of reaction will already be accounted for to a large degree in the thermodynamic properties of the components being mixed.

It is important to note that under the range of  $T$ ,  $P_{O_2}$ , and  $P_{SO_3}$  considered here,  $CoO$  and  $Cr_2O_3$  will be stable relative to their sulfates [25, 26], and therefore the superalloy chemical solution problem may be treated in two stages: (1) formation of an oxide film, and (2) chemical solution of the oxide film in the salt phase. The solubility of  $CoO$  and  $Cr_2O_3$  in sodium sulfate and sodium vanadate melts is thus of central importance. Four ternary systems are of interest:  $CoO-Na_2O-SO_3$ ,  $CoO-Na_2O-V_2O_5$ ,  $Cr_2O_3-Na_2O-SO_3$ , and  $Cr_2O_3-Na_2O-V_2O_5$ .

#### B. System $CoO-Na_2O-SO_3$

Deanhardt and Stern [27] have determined the solubility of  $CoO$  in molten  $Na_2SO_4$  at 1200 K (727 °C) as indicated in Fig. 5. Solubility varies markedly with  $A_{Na_2O}$  and reaches a minimum of about 100 ppm at about  $P_{SO_3} = 10^{-7}$ , near the minimum  $P_{SO_3}$  encountered in our modeling calculations. At the other extreme near  $P_{SO_3} = 10^{-4}$  atm, solubility of  $CoO$  would be close to 10 wt.%, using the extrapolated portion of the curve in Fig. 5. However the data in Fig. 5 apply to  $P_{O_2} = 0.2$  atm., somewhat higher than that prevailing under the modeling conditions used here.

C. System CoO-Na<sub>2</sub>O-V<sub>2</sub>O<sub>5</sub>

No experimental data are available for the solubility of CoO in sodium vanadate, based on a comprehensive literature search completed in late 1986.

D. System Cr<sub>2</sub>O<sub>3</sub>-Na<sub>2</sub>O-SO<sub>3</sub>

Zhang [28] has published data on the solubility of Cr<sub>2</sub>O<sub>3</sub> in fused Na<sub>2</sub>SO<sub>4</sub> at 1200 K at various oxygen pressures. An extrapolated curve corresponding to 7 x 10<sup>-2</sup> atm., the P<sub>O<sub>2</sub></sub> prevailing under the conditions of the model calculations, is given in Fig. 6. A marked variation in Cr<sub>2</sub>O<sub>3</sub> solubility as a function of P<sub>SO<sub>3</sub></sub>, with a pronounced minimum, is evident in Fig. 6. The minimum is about 100 ppm at a P<sub>SO<sub>3</sub></sub> of about 10<sup>-2</sup> atm., a pressure well above the conditions prevailing during our model calculations. The implication of Fig. 6 is that solubility of Cr<sub>2</sub>O<sub>3</sub> in Na<sub>2</sub>SO<sub>4</sub> is extensive under the range of P<sub>SO<sub>3</sub></sub> prevailing during the model calculations.

E. The System Cr<sub>2</sub>O<sub>3</sub>-Na<sub>2</sub>O-V<sub>2</sub>O<sub>5</sub>

Of the four ternary phase diagrams needed for oxide solubility, this is the only one for which direct data [29] are available. The 700 and 900 °C isotherms of the Cr<sub>2</sub>O<sub>3</sub> saturation surface shown in Fig. 7 apply to highly oxidizing conditions.

F. Estimates of Equilibrium Oxide Solubilities

From Fig. 7, it is apparent that over the range of V<sub>2</sub>O<sub>5</sub>/Na<sub>2</sub>V<sub>2</sub>O<sub>6</sub> ratios encountered in Appendix A, oxide solubilities do not vary appreciably. Thus to a first approximation at 700 °C, the sodium vanadate melt dissolves about 45 mol% Cr<sub>2</sub>O<sub>3</sub> and at 900 °C, it dissolves about 55 mol% Cr<sub>2</sub>O<sub>3</sub>. If we assume,

based on Fig. 6, that the same holds true for the sulfate melts, then as a very approximate estimate, molten salts in the system  $V_2O_5-Na_2V_2O_6-Na_2SO_4$  dissolve about 45 to 55 mole %  $Cr_2O_3$  at equilibrium under the conditions of the model calculations; for the initial stages of model development, 50 mole% will be used a test value. We do not have sufficient data to make an estimate of  $CoO$  solubility under the conditions of the model calculations, but this may not be a serious handicap in the early stages of model development, as  $Cr_2O_3$  dissolution is probably a major limiting factor in superalloy attack.

## VI. CHEMICAL KINETICS

### A. Methodology

Given that  $Co, Cr$  oxides are stable relative to sulfates under our model conditions, formation of an oxide film is assumed to be the first step in superalloy reaction:



It is assumed that the salt layer is thin, mobile and gas permeable so that the  $P_{O_2}$  is everywhere that in the gas, i.e., at about  $7 \times 10^{-2}$  atm. The formation of  $CoO$  and  $Cr_2O_3$  layers is than assumed to occur according to a simple parabolic rate law:

$$(M/A)^2 = kt,$$

where M is mass, A is area, t is time and k is the parabolic rate constant.

It is further assumed that solution of the oxide in the available salt is a relatively rapid process, by comparison with film growth. This seems reasonable given the highly fluid nature of the salt melts, and the undersaturated condition of the as-precipitated salt.

### B. Rate of Oxide Film Formation and Dissolution

Mrowec and Przybylski [30] have measured parabolic rate constants for the oxidation of cobalt to CoO at various oxygen partial pressures and temperatures. Under the conditions of our modeling calculations, a reasonable value of the parabolic rate constant for Co oxidation to CoO is  $10^{-9}$  g<sup>2</sup>/cm<sup>4</sup>·s. Birks and Meir [31] give an order of magnitude estimate of the parabolic rate constant for chromium oxidation to Cr<sub>2</sub>O<sub>3</sub> as  $10^{-11}$  g<sup>2</sup>/cm<sup>4</sup>·s. Clearly formation of Cr<sub>2</sub>O<sub>3</sub> is the slower of the oxidation processes, providing further justification for assuming, to a first approximation, that it is the chemical behavior of this component which has the largest effect on superalloy corrosion rates. Fig. 8 shows a hypothetical growth curve for Cr<sub>2</sub>O<sub>3</sub> film on pure Cr calculated using the above rate constant. The requirement for steady state is that the growth rate of the film is equal to the rate of chemical solution in the molten salt precipitate. Fig. 9 shows a plot of steady state mass removal rate vs. film thickness for the hypothetical case of a perfectly adherent film of Cr<sub>2</sub>O<sub>3</sub> on chromium. It is apparent that to remove material at a reasonable rate of a few mg/cm<sup>2</sup>/h would require very thin oxide films of submicron thickness.

## VII. CHEMICAL CORROSION MODEL

### A. Preliminary Test of Model

By assuming submicron thick steady state Cr<sub>2</sub>O<sub>3</sub> films and combining information on rate of oxide film removal from Fig. 9 with estimates of salt deposition rates from Table 5, it is clearly seen that, allowing for the effect of Cr dilution in the superalloy and assuming 50 mole % solution of the oxide in the salt phase, corrosion rates in the range 0.1 to 50 mg/cm<sup>2</sup>/h are readily

attainable. These are in reasonable agreement with the range of test-rig data of ref. [32].

#### B. Discussion and future Plans

It appears that our integrated chemical corrosion model, though an oversimplification at this stage of development, has sufficient flexibility to produce a large range of reasonable corrosion rates, based solely upon the equilibrium solution chemistry. It therefore appears advisable to proceed in this direction, by attempting to make the model fully quantitative. This will require additional phase equilibrium and solubility data for the system  $\text{Na}_2\text{V}_2\text{O}_6$ - $\text{Na}_2\text{SO}_4$ - $\text{V}_2\text{O}_5$ - $\text{CoO}$ - $\text{Cr}_2\text{O}_3$ . Also it will be necessary to modify the CFBL program to calculate simultaneously precipitation rates of more than one salt species.

There are a number of features observed experimentally which future modeling efforts should address. The formation of a sulfide layer is not consistent with the equilibrium chemistry presented here, and may require application of the principles of local equilibrium and mass transport at the metal interface. Also, an intergranular component seems to be prevalent in high temperature hot corrosion. It is possible that an intergranular chemical solution approach could be useful here as well and could be related directly to the processes of physical removal of metal from the walls.

#### VIII. ACKNOWLEDGEMENTS

The authors wish to express their appreciation to Dr. Dasara Rathnamma for her encouragement in this project. Discussion with Drs. Robert Jones and Kurt

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X. TABLES

Table 1. Impurity Concentration in Navy Test Fuels

<u>Fuel (Composition)</u>	<u>Na (ppm. wt.)</u>	<u>S (wt%)</u>	<u>V (ppm. wt.)</u>
Base Fuel ( $\text{CH}_{2.0}$ )	1.0	0.07	0.5
GT 10 ( $\text{CH}_{1.8}$ )	1.0	1.0	0.5
GT 12 ( $\text{CH}_{1.8}$ )	2.0	2.0	2.0

Table 2. Matrix of Fuel Impurity Concentrations Used in Concentrations Used in Modeling

	<u>Na (ppm. wt.)</u>	<u>S (wt. %)</u>	<u>V (ppm. wt.)</u>
(1)	0.1	0.01	0.1
(2)	1.0	0.1	1.0
(3)	10.0	1.0	10.0

TABLE 3. Species Considered by GEC

L 5/66	AR	J 3/78	C	J 12/67	CH	J 12/72	CH2	J 3/61	CH2O
L 5/80	CH2O2	J 6/69	CH3	BUR 84	CH2OH	L 6/80	CH3O	L 5/84	CH4
L 4/80	CH3OH	J 6/69	CN	J 12/70	CN2	J 6/66	CNN	J 9/65	CO
J 3/61	COS	J 9/65	CO2	J 12/76	CS	J 12/76	CS2	J 12/69	C2
J 3/67	C2H	J 3/61	C2H2	BUR 84	C2H3	L 4/80	C2H4	L 5/80	C2H4O2
L 5/80	C2H4O4	A10/83	C2H5	L 5/84	C2H6	BUR 84	CH3N2CH3	BUR 84	C2H5OH
BUR 84	CH3OCH3	J 3/67	C2N	J 3/61	C2N2	J 9/66	C2O	J 12/69	C3
L11/80	C3H6O	BUR 84	N-C3H7	BUR 84	I-C3H7	L 4/80	C3H8	L 1/84	1-C3H7OH
J 6/68	C3O2	J 12/69	C4	L 5/80	C4H8O4	L 4/80	N-C4H10	L 5/80	I-C4H10
J 3/61	C4N2	J 12/69	C5	L 1/84	C6H5	L 4/84	C6H5O	L 1/84	C6H6
L 4/84	C6H5OH	BUR 84	C7H8	P12/52	C8H16	P 4/81	N-C8H18	P10/74	I-C8H18
L 1/84	O-C12H9	L 4/84	C12H10	J 3/77	H	L12/69	HCN	J 12/70	HCO
J 12/70	HNCO	J 3/63	HNO	J 6/63	HN02	J 6/63	HN03	J 9/78	HO2
J 3/77	H2	J 12/65	H2N2	J 3/79	H2O	L 6/80	H2O2	J 6/77	H2S
J 9/77	H2SO4	J 3/77	N	J 12/70	NCO	J 6/77	NH	J 6/77	NH2
J 6/77	NH3	J 6/63	NO	J 9/64	NO2	J 12/64	NO3	J 3/77	N2
J 12/65	N2H4	J 12/64	N2O	J 9/64	N2O4	J 12/64	N2O5	J 12/70	N3
J 6/62	NA	J 3/66	NACN	J 3/63	NAH	J 12/67	NAO	J 12/70	NAOH
J 6/62	NA2	J 3/66	NA2C2N2	K10/74	NA2O	J 12/70	NA2O2H2	J 6/78	NA2S04
J 3/77	O	J 6/77	OH	J 3/77	O2	J 6/61	O3	J 9/77	S
J 6/77	SH	J 6/61	SN	J 6/77	SO	J 6/61	SO2	J 9/65	SO3
J 9/77	S2	J 9/65	S2O	J 6/64	S8	J 6/73	V	J 12/73	VN
J 12/73	VO	J 12/73	VO2	J 3/78	C(GR)	P10/80	C7H8(L)	P10/80	C8H18(L)
L 3/81	H2O(S)	J 3/79	H2O(L)	J 9/77	H2SO4(L)	J 12/73	VN(S)	BAR 77	N2H8S04(S)
J 6/62	NA(S)	J 6/62	NA(L)	J 3/66	NACN(S)	J 3/66	NACN(L)	J 12/70	NAOH(A)
J 12/70	NAOH(L)	J 6/63	NAO2(S)	J 3/66	NA2CO3(1)	J 3/66	NA2CO3(2)	J 3/66	NA2CO3(L)
J 6/68	NA2O(C)	J 6/68	NA2O(A)	J 6/68	NA2O(L)	J 6/68	NA2O2(A)	J 6/68	NA2O2(B)
J 3/78	NA2S(1)	J 3/78	NA2S(2)	J 3/78	NA2S(L)	BAR 77	NA2S03(S)	BAR 77	NA2S03(L)
J 6/78	NA2SO4(IV)	J 6/78	NA2SO4(I)	J 6/78	NA2S04(L)	J 9/77	S(S)	J 9/77	S(L)
J 6/73	V(S)	J 6/73	V(L)	KDA 84	NAV308(S)	KDA 84	NA2V12031(S)	KDA 84	NA2V12031(L)
BAR 73	NA2V206(S)	BAR 73	NA2V206(L)	BAR 73	NA4V207(S)	BAR 73	NA6V208(S)	BAR 73	NA6V208(L)
BAR 73	VO(S)	BAR 73	VO(L)	BAR 73	VO2(S)	BAR 73	VO2(S)	BAR 73	VO2(L)
BAR 73	V203(S)	BAR 73	V203(L)	BAR 73	V205(S)	BAR 73	V205(L)		

TABLE 4. Coefficients for  $V_4O_{10}$   
(CEC format)

Based on Semenov, et al [1970]

V4O10	<u>SB1/87V</u>	40	10	0	0G	300.000	5000.000	1
0.45894528E+02	0.0		0.0		0.0		0.0	2
-0.36143218E+06	-0.22261447E+03		0.45894528E+02	0.0			0.0	3
3.0	-0.36143218E+06	-0.22261447E+03						4

Based on Polyakov [1946]

V4O10	<u>PB1/87V</u>	40	10	0	0G	300.000	5000.000	1
0.45894528E+02	0.0		0.0		0.0		0.0	2
-0.35802894E+06	-0.21333830E+03		0.45894528E+02	0.0			0.0	3
3.0	-0.35802894E+06	-0.21333830E+03						4

Table 5. CFBL Salt Deposition Rates

Composition Code	T = 1172 K P = 1 atm Liquid Mole Fractions			Salt Deposition Rate (mg/h/cm <sup>2</sup> )
	$Na_2SO_4$	$Na_2V_2O_6$	$V_2O_5$	
131	0.01433	0.87555	0.11011	0.1611
231	0.33446	0.6618	0.0036	0.0451
331	0.99378	0.0061	0.0000	0.3542
132	0.0005	0.20862	0.79091	8.574
232	0.15898	0.83149	0.0094	0.1804
332	0.93993	0.059908	0.0001	0.3787
133	0.0000	0.02181	0.97815	105.304
233	0.0005	0.21967	0.77982	84.1427
333	0.48135	0.51653	0.0019	0.8106

TABLE 6. CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

CASE NO. 8701 131 0.1 ppm Na, 1%S, 0.1 ppm V

V1ROP1HT

## - - INPUT PARAMETERS

- -

(ALL GAS PROPERTIES PERTAIN TO TJ, PJ)

RUN = 19  
 $T_0 \langle K \rangle = 1806.000$  TYPE = 0  
 $T_W \langle K \rangle = 1172.000$   $P_0 \langle ATM \rangle = 1.068000$   
Fuel/Air Mass Ratio (F)  $P_J \langle ATM \rangle = 1.000000$   
Air Flow Rate (WA, G/SEC) = 0.045380  
Dia. Cyl. Target (DIAW, CM) = 2.940000  
Length (hgt) Target (LW, CM) = 0.318000  
Dia. Jet Nozzle (DJ, CM) = 3.810000  
Observed Deposition rate (W0BS, MG/HR) = 6.033000  
FSORET? = T TURB = 0.0000 PERCENT  
TURL (CM) = 0.000000 PERCENT

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

D(I)	NU(I)	SC(I)	X(I)	X(I), W	TAU(I)	F(SORET), I	M(I)
1 0.27773E+01	0.39893E+01	0.10853E+01	0.50180E-08	0.13280E-08	0.45016E-01	1.02268	0.89010E-03
2 0.35112E+01	0.36321E+01	0.85843E+00	0.41340E-09	0.00000E+00	-0.15846E-01	0.99210	0.10953E-03
3 0.17005E+01	0.48542E+01	0.17725E+01	0.14160E-16	0.95190E-09	0.17019E+00	1.08751	-0.29915E-03
6 0.23382E+01	0.42736E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.92532E-01	1.04698	0.00000E+00

YNAJ YNAW YSJ YSW  
0.543140E-08 0.323180E-08 0.394772E-03 0.394881E-03

Average Molec. Wt. = 28.81275  
Turbulence factor = 1.000000

Re(EFF) = 57.533  
Total Na mass flux to surface (SUM,  $G/CM^{**2}/SEC$ ) = 1.65482E-11  
Total S mass flux to surface (SMS,  $G/CM^{**2}/SEC$ ) = 3.92336E-07  
Na-to-S molar flux ratio at the surface = 0.0001

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 7.00474E-04  
ERROR (\*) = -8.443E+01

GM = 1.26949  
TJ (K) = 1780.95  
PR = 0.690190  
MOLE FRACTIONS  
X(N2) = 0.755099  
X(O2) = 0.065770  
X(H2O) = 0.089565  
X(CO2) = 0.089565

RHOJ(G/CM\*\*3) UJ(CM/S) ETAMIX(POISE) LAMIX(CAL/CM/K/S) CMIX(CAL/G/S)  
0.197159E-03 0.545317E+03 0.594261E-03 0.279215E-03 0.324288E+00

XI. ILLUSTRATIONS

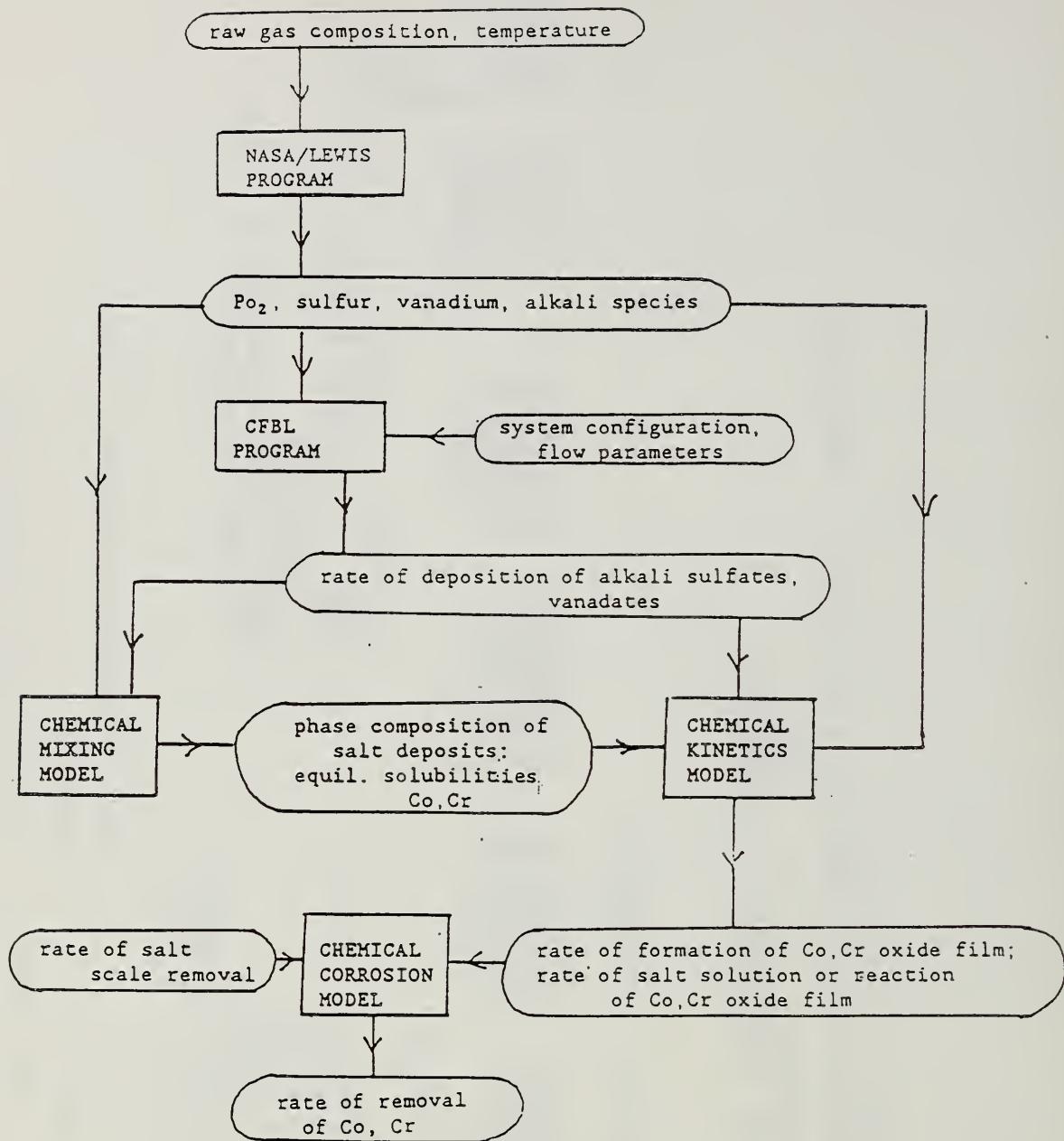


Figure 1. Flow chart of molten salt/superalloy corrosion model.

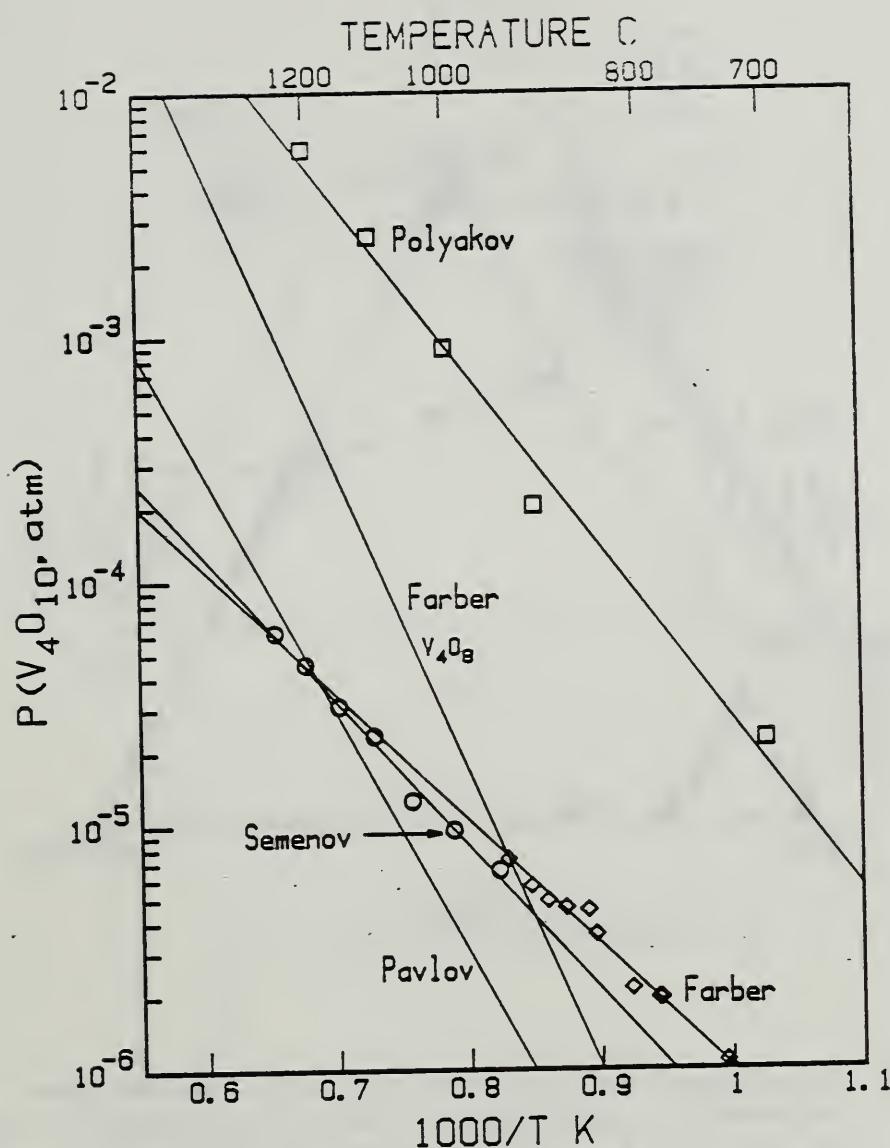


Figure 2. Partial pressures of species in the system V-O. Data from Polyakov [18], Semenov et al. [19], and Farber et al. [20]. Data and curves are for  $2V_2O_5(c) = V_4O_{10}(g)$ , except "Farber  $V_4O_8$ ", which is presumably a decomposition process. Only the Farber data are species specific measurements.

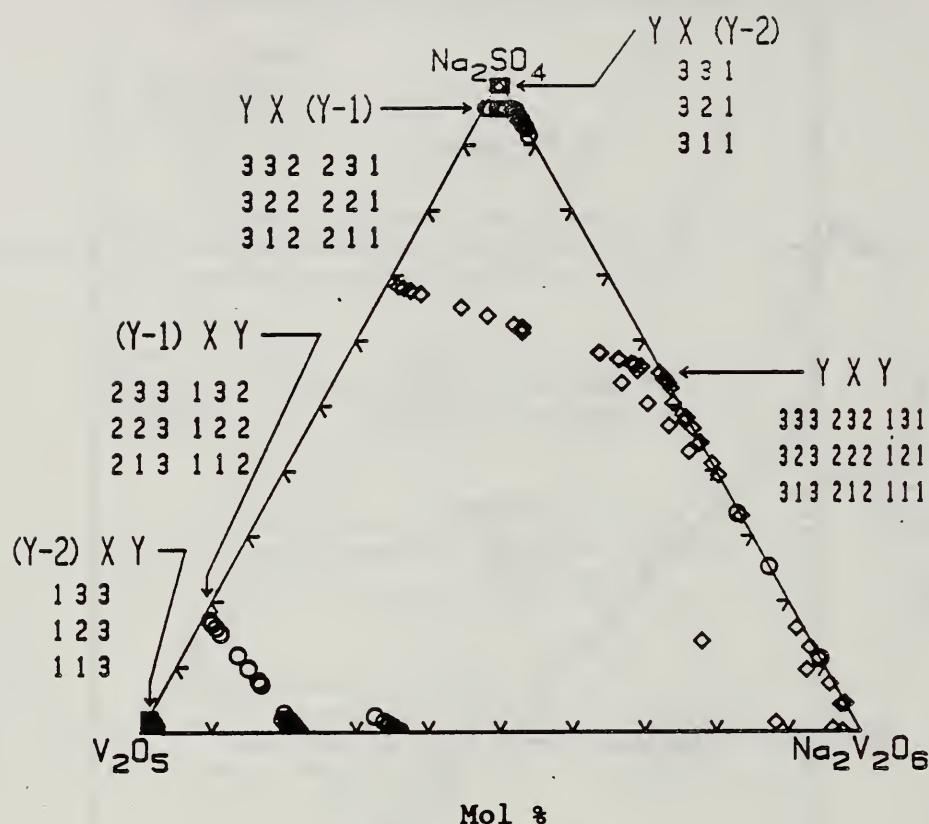


Figure 3. Calculated equilibrium molten salt compositions produced by combustion of fuels with impurity levels as in Table 2. Calculations completed at 977 and 1172 K and at 1, 5, 10 and 15 atm (see Appendix A).

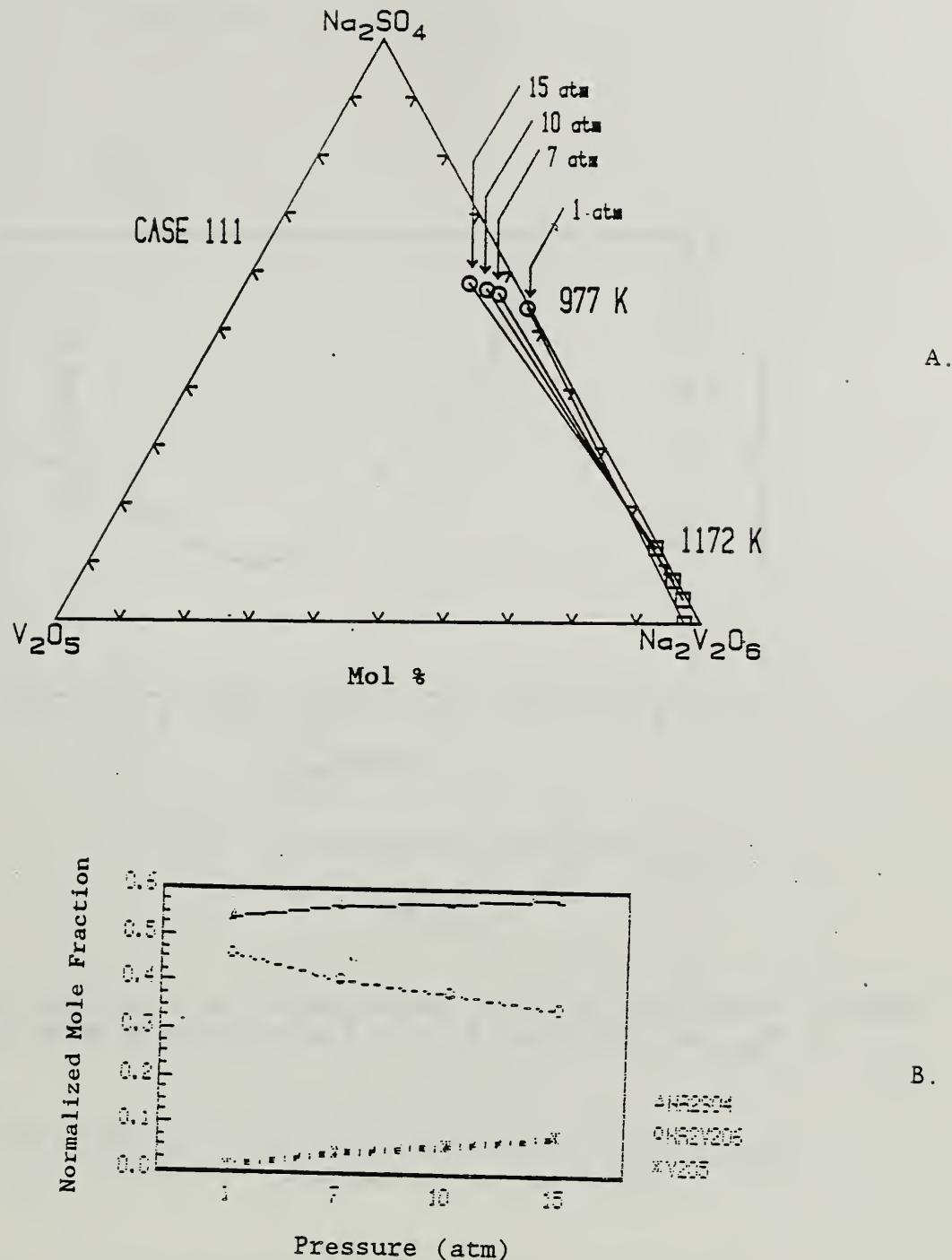


Figure 4. Effect of pressure and temperature on molten salt composition produced from (111) fuel (0.1 ppm Na, 0.01 wt% S, 0.1 ppm V). A) ternary plot.  
B) effect of pressure at constant temperature ( 977 K ).

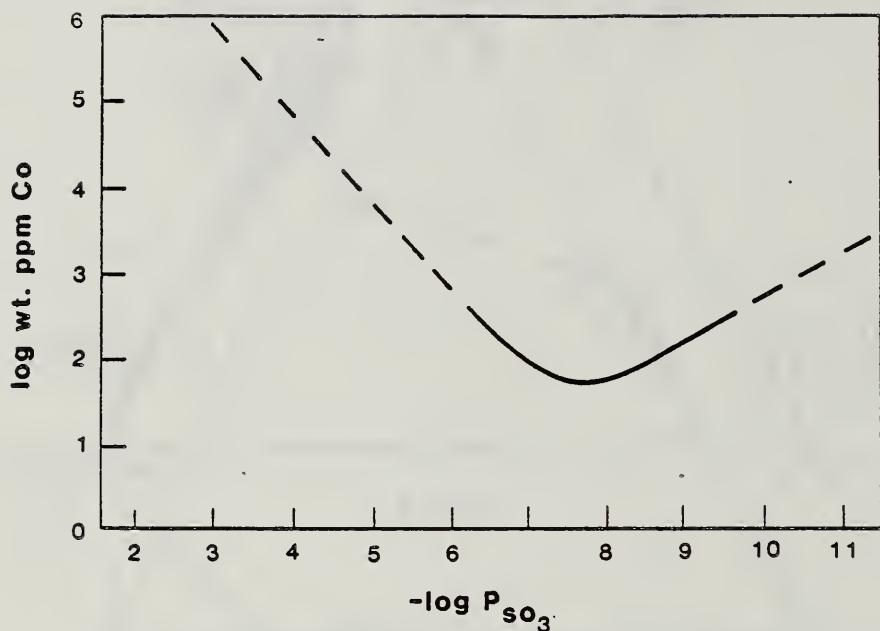


Figure 5. Solubility of CoO in molten Na<sub>2</sub>SO<sub>4</sub> as a function of P<sub>SO<sub>3</sub></sub> at 1200 K and P<sub>O<sub>2</sub></sub> = 0.2 atm (modified after ref [27]).

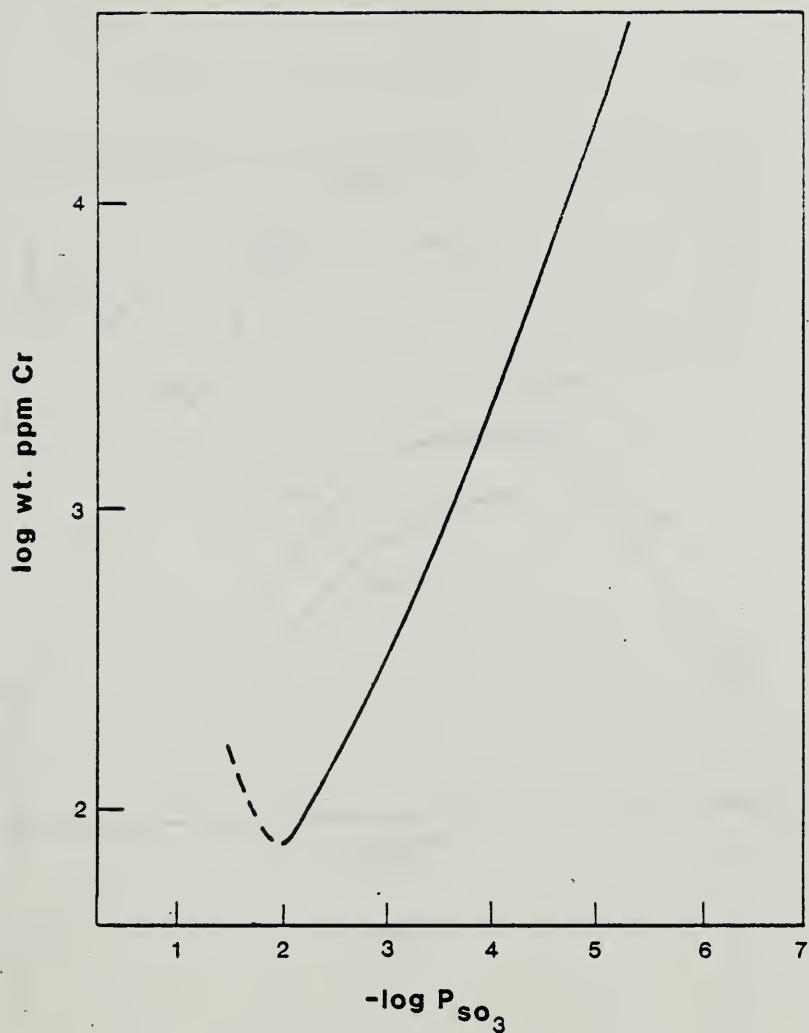


Figure 6. Solubility of  $\text{Cr}_2\text{O}_3$  in molten  $\text{Na}_2\text{SO}_4$  at 1200 K and  $\text{P}_{\text{O}_2} \sim 7 \times 10^{-2}$  atm. (modified after ref [28]).

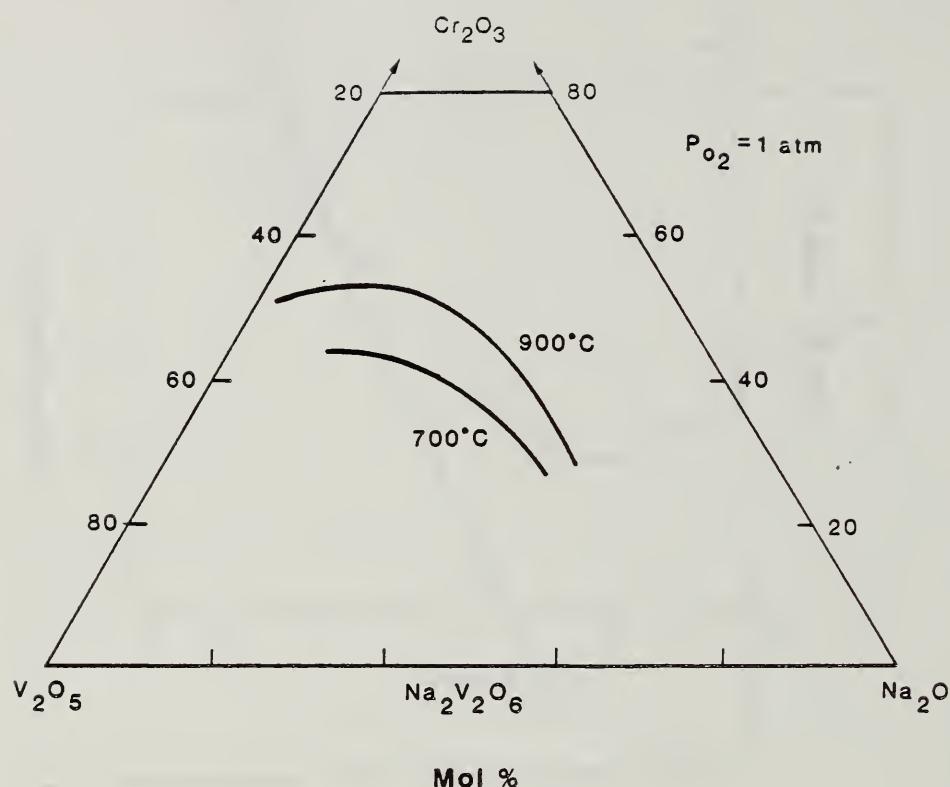


Figure 7. Solubility isotherms for  $\text{Cr}_2\text{O}_3$  in sodium vanadate melts at 700° and 900 °C (modified after ref [29]).

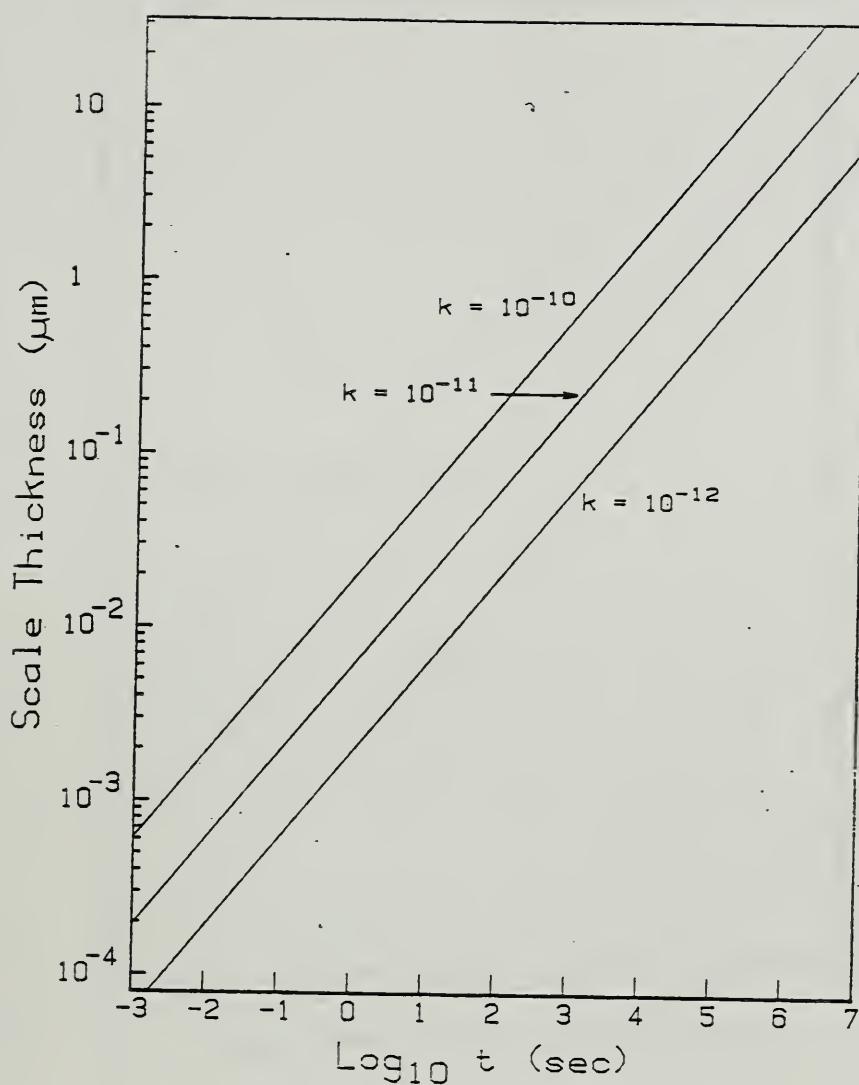


Figure 8. Calculated growth curves of  $\text{Cr}_2\text{O}_3$  film on Cr metal for various parabolic rate constants.

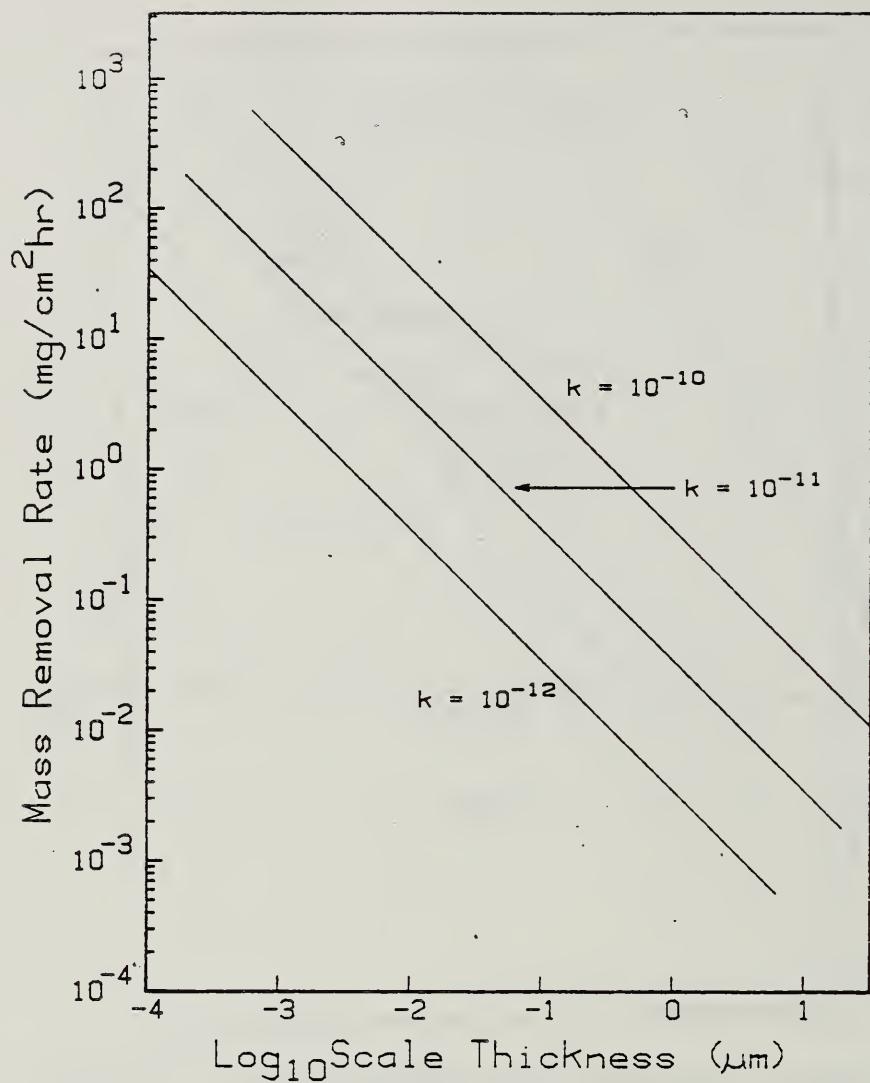


Figure 9. Film thickness vs. steady state mass removal rate for  $\text{Cr}_2\text{O}_3$  film on Cr for the three different rate constants of Fig. 8.

XII. APPENDICES

Appendix A. CEC calculations of gas/condensed phase equilibria for fuels with various impurity levels (see Table 2).



CASE NO. 8701 211 0.01% SULFUR, 1.0 MA, 0.1 V PPM

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P, ATM 1.0000

T, DEG K 1172.0

SOLUTION 1

AR 8.8005-3

CO 3.0982-9

CO2 9.0898-2

H 5.974-12

HNO 1.515-12

HNO2 4.1197-9

HNO3 1.205-11

HO2 1.1950-8

H2 2.6144-9

H2O 9.6947-2

H2O2 4.817-10

H2SO4 2.726-11

NO 9.4443-5

NO2 1.0011-6

N2 7.3499-1

N2O 5.5982-9

NA 4.788-12

NaOH 3.7017-8

Na2SO4 7.3506-9

O 3.4941-9

OH 1.5471-6

O2 6.6260-2

O3 1.882-12

SO2 3.6710-6

SO3 3.0849-7

M, MOL WT 28.868

PHASE FRACTION 1.0000 0

SOLUTION 2

NaOH(L) 3.0668-5

Na2O(C) 1.974-12

Na2SO3(L) 4.005-10

Na2SO4(L) 1.1066-1

Na2V2O6(L) 8.8194-1

Na4V2O7(S) 7.2248-3

Na6V2O8(S) 2.9827-7

V2O3(S) 4.497-10

V2O5(L) 1.4382-4

M, MOL WT 233.02

PHASE FRACTION 1.3831-9

## PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C CH CH2 CH2O CH2O2 CH3 CH2OH CH3O CH4 CH

CN CH2 CNH COS CS CS2 C2 C2H C2H2 C2

C2H4 C2H4O2 C2H4O4 C2H5 C2H6 CH3CH2CH3 C2H5OH CH3OCH3 C2N C2

C2O C3 CH3O H-C3H7 I-C3H7 C3H8 1-C3H7OH C3O2 C4 C4

H-C4H10 I-C4H10 C4H2 CS C4H5 C4H5O C4H6 C4H5OH C7H8 C8

H-C8H18 I-C8H18 O-C12H9 C12H10 HCO HCO HNO2 H2O2 H2S N

NCO NH NH2 NH3 NO3 NO2 NO2 NO2 NO3 NO

NAH NaO Na2 Na2C2H2 Na2O Na2O2H2 S SH SH SH SO

S2 S2O S8 V VN VO VO2

SOLUTION 2

NaOH(A) Na2O(A) Na2O(L) Na2SO3(S) Na2SO4(IV) Na2SO4(I) Na2V2O6(S) Na6V2O8(L) V2O3(L) V2

PURE SPECIES

C16R C7H8(L) C8H18(L) H2O(S) H2O(L) H2SO4(L) VN(S) Na2HSO4(S) Na(S) Na

NaOH(S) NaOH(L) NaO2(S) Na2O3(I) Na2O3(2) Na2O3(L) Na2O2(A) Na2O2(B) Na2S(I) Na

Na2S(L) S(S) S(L) V(S) V(L) Na3O8(S) Na2V12O31(S) Na2V12O31(L) VO(S) VO

VO2(S) VO2(S) VO2(L)

CASE NO. 8701 311 0.01% SULFUR, 10 NA, 0.1 V PPM TIME = 0.520 SEC  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

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SOLUTION 1

AR 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3  
 CO 3.0980-9 9.536-12 1.3860-9 4.265-12 1.1710-9 3.504-12 9.797-10 3.015-12 8.000-10 2.462-12  
 CO2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2  
 H 5.874-12 4.834-15 1.757-12 1.446-15 1.385-12 1.123-15 1.045-12 9.596-16 7.707-13 6.342-16  
 HNO 1.515-12 1.651-14 2.265-12 2.469-14 2.464-12 2.686-14 2.694-12 2.936-14 2.981-12 3.250-14  
 HNO2 4.1199-9 1.6059-9 1.3775-8 5.3895-9 1.7729-8 6.9107-9 2.3167-8 9.0303-9 3.1400-8 1.2240-8  
 HNO3 1.205-11 1.509-11 9.011-11 1.128-10 1.372-10 1.718-10 2.143-10 2.683-10 3.558-10 4.454-10  
 H2O 1.1950-8 9.702-10 1.7870-8 1.4510-9 1.9440-8 1.5780-9 2.1250-8 1.7250-9 2.3520-8 1.9090-9  
 H2- 2.6140-9 1.618-11 1.1690-9 7.234-12 9.881-10 6.114-12 8.267-10 5.116-12 6.750-10 4.177-12  
 H2D 9.6946-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2  
 H2O2 4.817-10 5.487-11 1.0770-9 1.227-10 1.2750-9 1.452-10 1.5230-9 1.735-10 1.8660-9 2.125-10  
 H2SO4 2.584-11 7.696-10 2.602-10 5.8380-9 4.186-10 8.7350-9 6.899-10 1.3290-8 1.2100-9 2.1210-8  
 NO 9.4444-5 1.4817-5 9.4443-5 1.4817-5 9.4442-5 1.4817-5 9.4442-5 1.4817-5 9.4441-5 1.4817-5  
 NO2 1.0011-6 5.1937-7 2.2386-6 1.1613-6 2.6487-6 1.3741-6 3.1658-6 1.6423-6 3.8772-6 2.0114-6  
 NO3 1.255-13 2.775-14 6.274-13 1.387-13 8.784-13 1.942-13 1.255-12 2.774-13 1.882-12 4.162-13  
 N2 7.3899-1 7.3703-1 7.3899-1 7.3703-1 7.3899-1 7.3704-1 7.3899-1 7.3704-1 7.3899-1 7.3704-1  
 N2O 5.5983-9 1.0091-9 1.2518-8 2.2564-9 1.4811-8 2.6698-9 1.7703-8 3.1910-9 2.1682-8 3.9081-9  
 NA 1.472-11 4.811-17 6.215-13 2.337-18 3.218-13 1.254-18 1.605-13 6.512-19 7.303-14 3.105-19  
 NAO 1.750-12 9.350-18 1.652-13 1.015-18 1.012-13 6.449-19 6.034-14 4.001-19 3.362-14 2.337-19  
 NAOH 1.1380-7 1.507-11 1.6070-8 2.446-12 1.0710-8 1.690-12 6.9780-9 1.147-12 4.3030-9 7.410-13  
 NA2SO4 6.5870-8 1.116-10 1.3220-8 2.232-11 9.4430-9 1.594-11 6.6110-9 1.116-11 4.4080-9 7.440-12  
 O 3.4940-9 1.966-11 1.5630-9 8.794-12 1.3210-9 7.432-12 1.1050-9 6.218-12 9.022-10 5.077-12  
 OH 1.5471-6 5.5773-8 1.0346-6 3.7297-8 9.5112-7 3.4238-8 8.6998-7 3.1363-8 7.8611-7 2.8340-8  
 O2 6.6261-2 6.6301-2 6.6320-2 6.6320-2 6.6320-2 6.6320-2 6.6259-2 6.6300-2 6.6258-2 6.6279-2  
 O3 1.882-12 9.957-14 4.208-12 2.226-13 4.979-12 2.634-13 5.751-12 3.149-13 7.288-12 3.854-13  
 SO2 3.4802-6 2.2968-6 3.1345-6 1.5583-6 3.0439-6 1.4075-6 2.9379-6 1.2539-6 2.8041-6 1.0873-6  
 SO3 2.9246-7 1.4182-6 5.8899-7 2.1515-6 6.7676-7 2.2994-6 7.8069-7 2.4484-6 9.1261-7 2.6051-6  
 M, MOLE WT 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

SOLUTION 2

NAOH(L) 9.4291-5 6.6079-7 6.6555-5 5.3648-7 6.2094-5 5.1875-7 5.7815-5 5.0291-7 5.3476-5 4.8756-7  
 NA2O(C) 1.828-11 0.000 0 1.822-12 0.000 0 1.133-12 0.000 0 0.000 0 0.000 0 0.000 0  
 NA2SO3(S) 0.000 0 9.082-12 0.000 0 4.062-12 0.000 0 3.433-12 0.000 0 2.872-12 0.000 0 2.345-12  
 NA2SO3(L) 3.5890-9 0.000 0 1.6110-9 0.000 0 1.3610-9 0.000 0 1.1370-9 0.000 0 9.301-10 0.000 0  
 NA2SO4(I) 0.000000 9.7548-1 0.000000 9.7548-1 0.000000 9.7548-1 0.000000 9.7548-1 0.000000 9.7548-1  
 NA2SO4(L) 9.9169-1 0.000000 9.7504-1 0.000000 9.7517-1 0.000000 9.7526-1 0.000000 9.7532-1 0.000000  
 NA2V2O6(L) 7.6267-3 4.4959-3 4.8563-3 4.3743-3 4.7479-3 4.3084-3 4.6708-3 4.2067-3 4.6128-3 4.0460-3  
 NA4V2O7(S) 5.9058-4 2.2280-7 3.7472-5 2.8577-8 2.2777-5 1.8812-8 1.3578-5 1.2081-8 7.6573-6 7.2770-9  
 NA6V2O8(S) 2.2270-7 0.000 0 1.4080-9 0.000 0 5.322-10 0.000 0 1.928-10 0.000 0 6.194-11 0.000 0  
 V2O5(L) 1.3157-7 1.8752-5 8.4075-7 1.3839-4 1.3221-6 2.0375-4 2.1432-6 3.0306-4 3.7110-6 4.6497-4  
 M, MOLE WT 142.90 142.50 142.53 142.49 142.52 142.48 142.51 142.48 142.50 142.47  
 PHASE FRACTION 1.4967-7 2.7243-7 2.5129-7 2.7256-7 2.5775-7 2.7258-7 2.6245-7 2.7261-7 2.6599-7 2.7266-7

PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH2OH	CH3O	CH4	CH
CN	CN2	CNN	COS	CS	C5	C2	C21	C22	C2
C2H4	C2H402	C2H404	C2H5	C2H6	C3H2C4H3	C2H5OH	CH3OCH3	C2N	C2
C2O	C3	C3H60	N-C3H7	I-C3H7	C3H8	1-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4N2	C5	C4H5	C6H50	C6H6	C6H5OH	C7H8	C8
N-C8H18	I-C8H18	O-C12H9	C12H10	HCO	HCO	HCO	H2K2	H2S	N
NCO	NH	NH2	NH3	N2H4	N2O4	N2O5	N3	NACN	NA
NA2	NA2C2H2	NA2O	NA2O2H2	S	SH	SN	SD	S2	S2
SB	V	VN	VO	VO2					

SOLUTION 2

NAOH(A)	NA2O(A)	NA2O(L)	NA2SO4(IV)	NA2V2O6(S)	NA6V2O8(L)	V2O3(S)	V2O3(L)	V2O5(S)	
PURE SPECIES									
C16R	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	N2H6SO4(S)	NA(S)	NA
NAON(S)	NAON(L)	NAO2(S)	NA2CO3(I)	NA2CO3(2)	NA2CO3(L)	NA2O2(A)	NA2O2(B)	NA2S(I)	NA
NA2S(L)	S(S)	S(L)	V(S)	V(L)	NAV3O8(S)	NA2V12O31(S)	NA2V12O31(L)	VO(S)	VO
V2O(S)	V2O2(S)	V2O(L)							

CASE NO. 8701 112 0.01% SULFUR, 0.1 NA, 1.0 V PPM TIME = 0.512 SEC  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

## SOLUTION 1

AR 8.8005-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3  
 CO 3.0989-9 9.536-12 1.386-9 4.285-12 1.1710-9 3.604-12 9.798-10 3.016-12 8.000-10 2.462-12  
 CO2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2  
 H 5.874-12 4.834-15 1.757-12 1.446-15 1.365-12 1.123-15 1.045-12 8.596-16 7.707-13 6.342-16  
 HNO 1.515-12 1.451-14 2.285-12 2.469-14 2.464-12 2.686-14 2.694-12 2.736-14 2.981-12 3.250-14  
 HNO2 4.1197-9 1.6058-9 1.3775-8 5.3694-9 1.7729-8 6.9107-9 2.3166-8 9.0302-9 3.1400-8 1.2239-8  
 HNO3 1.205-11 1.509-11 9.011-11 1.128-10 1.372-10 1.718-10 2.143-10 2.683-10 3.558-10 4.454-10  
 HO2 1.1950-8 9.702-10 1.7870-8 1.4510-9 1.9440-8 1.5780-9 2.1250-8 1.7250-9 2.3520-8 1.9090-9  
 H2 2.6140-9 1.618-11 1.1690-9 7.235-12 9.882-10 6.114-12 8.268-10 5.116-12 6.751-10 4.177-12  
 H2O 9.6947-2 9.6948-2 9.6947-2 9.6948-2 9.6947-2 9.6948-2 9.6947-2 9.6948-2 9.6947-2 9.6948-2  
 H2O2 4.817-10 5.487-11 1.0770-9 1.227-10 1.2750-9 1.452-10 1.5230-9 1.735-10 1.8660-9 2.125-10  
 H2SO4 2.731-11 8.258-10 2.786-10 6.2640-9 4.486-10 9.3730-9 7.396-10 1.4260-8 1.2970-9 2.2750-8  
 NO 9.4443-5 1.4817-5 9.4442-5 1.4817-5 9.4442-5 1.4816-5 9.4441-5 1.4816-5 9.4441-5 1.4816-5  
 NO2 1.0011-6 5.1936-7 2.2385-6 1.1613-6 2.6487-6 1.3741-6 3.1657-6 1.6423-6 3.8772-6 2.0114-6  
 NO3 1.255-13 2.774-14 6.274-13 1.387-13 8.784-13 1.942-13 1.255-12 2.774-13 1.882-12 4.162-13  
 N2 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1  
 N2O 5.5982-9 1.0091-9 1.2518-8 2.2563-9 1.4811-8 2.6697-9 1.7703-8 3.1909-9 2.1681-8 3.9081-9  
 NaOH 2.449-10 5.172-13 1.113-10 2.259-13 9.424-11 1.985-13 7.898-11 1.547-13 6.456-11 1.223-13  
 Na2SO4 3.224-13 1.411-13 6.791-13 2.043-13 7.839-13 2.128-13 9.078-13 2.179-13 1.064-12 2.175-13  
 O 3.4940-9 1.966-11 1.5630-9 8.794-12 1.3210-9 7.432-12 1.1050-9 6.218-12 9.022-10 5.077-12  
 OH 1.5471-6 5.5772-8 1.0346-6 3.7297-8 9.5112-7 3.4288-8 8.6998-7 3.1363-8 7.8611-7 2.8340-8  
 O2 6.6260-2 6.6300-2 6.6259-2 6.6299-2 6.6299-2 6.6259-2 6.6299-2 6.6257-2 6.6299-2 6.6299-2  
 O3 1.882-12 9.957-14 4.208-12 2.226-13 4.979-12 2.634-13 5.951-12 3.148-13 7.289-12 3.856-13  
 SO2 3.6779-6 2.4645-6 3.3561-6 1.6721-6 3.2615-6 1.5103-6 3.1494-6 1.3454-6 3.0071-6 1.1688-6  
 SO3 3.0907-7 1.5217-6 6.3064-7 2.3086-6 7.2513-7 2.4673-6 8.3691-7 2.6271-6 9.7868-7 2.7951-6  
 M, MOLE WT 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

## SOLUTION 2

NaOH(L) 2.0290-7 2.2868-8 4.6102-7 4.9533-8 5.4635-7 5.7883-8 6.5434-7 6.7846-8 8.0233-7 8.0469-8  
 Na2SO4(I) 0.000000 1.2589-3 0.000000 9.1129-3 0.000000 1.3289-2 0.000000 1.7440-2 0.000000 2.9096-2  
 Na2SO4(L) 4.8530-6 0.000000 5.1119-5 0.000000 8.2611-5 0.000000 1.3666-4 0.000000 2.4027-4 0.000000  
 Na2V2O6(L) 2.1162-1 2.2005-1 2.1700-1 2.1045-1 2.1745-1 2.0535-1 2.1821-1 1.9784-1 2.1858-1 1.8604-1  
 Na2V2O6(I) 2.1162-1 2.2005-1 2.1700-1 2.1045-1 2.1745-1 2.0535-1 2.1821-1 1.9784-1 2.1858-1 1.8604-1  
 Na4V2O7(S) 7.5883-8 1.2852-8 8.0339-8 1.1730-8 8.0895-8 1.1155-8 8.1371-8 1.0335-8 8.1700-8 9.1146-8  
 V2O3(S) 2.4450-6 1.1510-6 4.8960-7 2.3270-9 3.4940-7 1.6640-9 2.4440-7 1.1670-9 1.6280-7 7.802-10  
 V2O5(L) 7.8837-1 7.7870-1 7.8295-1 7.8044-1 7.8227-1 7.8134-1 7.8166-1 7.8272-1 7.8119-1 7.8486-1  
 M, MOLE WT 195.00 195.47 195.33 194.56 195.37 194.08 195.40 193.37 195.42 192.25  
 PHASE FRACTION 1.2300-8 1.2315-8 1.2300-8 1.2413-8 1.2301-8 1.2465-8 1.2302-8 1.2344-8 1.2303-8 1.2668-8

## PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

## SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH20H	CH30	CH4	CH
CH	CH2	CH0	CH0	CS	CS2	C2	C2H	C2H2	C2
C2H4	C2H402	C2H404	C2H6	C2H402CH3	C2H50H	C2H30CH3	C2N	C2	
C20	C3	C3H60	M-C3H7	I-C3H7	C3H8	I-C3H70H	C3O2	C4	C4
M-C4H10	I-C4H10	C4N2	C5	C6H5	C6H50	C6H6	C6H50H	C7H8	C8
M-C8H18	I-C8H18	O-C12H9	C12H10	HCO	HCO	HCO	H2N2	H2S	N
NCO	NH	NH2	NH3	N2H4	N2O4	N2O5	N3	NA	NA
NAH	NA0	NA2	NA2C2H2	NA20	NA20H2	S	SH	SN	SD
S2	S20	S8	V	VN	VO	VO2			

## SOLUTION 2

NaOH(A)	Na2O(C)	Na2O(A)	Na2O(L)	Na2SO3(S)	Na2SO3(L)	Na2SO4(IV)	Na2V2O6(S)	Na4V2O8(S)	NA
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## V2O3(L)

## V2O5(S)

## PURE SPECIES

C(SR)	C7H8(L)	CH18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	H2BSO4(S)	NA(S)	NA
NaCN(S)	NaCN(L)	NaO2(S)	Na2CO3(I)	Na2CO3(2)	Na2CO3(L)	Na2O2(A)	Na2O2(B)	Na2S(I)	NA
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

CASE NO. 9701 212 0.012SULFUR, 1.0 MA, 1.0 V PPM TIME = 0.702 SEC  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

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SOLUTION 1

AR 8.8005-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3  
 CO 3.0890-9 9.534-12 1.384-9 4.265-12 1.1710-9 3.504-12 9.799-10 3.015-12 3.000-10 2.462-12  
 CO2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2 9.0898-2  
 H 5.374-12 4.334-15 1.757-12 1.446-15 1.365-12 1.123-15 1.045-12 3.596-16 7.707-13 5.342-16  
 HNO 1.515-12 1.651-14 2.265-12 2.469-14 2.444-12 2.686-14 2.694-12 2.936-14 2.981-12 3.250-14  
 HNO2 4.1197-9 1.6058-9 1.3775-8 5.3694-9 1.7729-8 5.9107-9 2.3166-8 9.0302-9 3.1400-8 1.2239-8  
 HNO3 1.205-11 1.509-11 9.011-11 1.129-10 1.372-10 1.719-10 2.143-10 2.683-10 3.558-10 4.454-10  
 H2O 1.1950-8 9.702-10 1.7870-8 1.4510-9 1.9440-8 1.5780-9 2.1250-8 1.7250-9 2.3520-8 1.9090-9  
 H2 2.6140-9 1.618-11 1.1690-9 7.233-12 9.882-10 6.114-12 8.268-10 5.116-12 6.750-10 4.177-12  
 H2O 9.6947-2 9.6948-2 9.6947-2 9.6948-2 9.6947-2 9.6948-2 9.6947-2 9.6948-2 9.6947-2 9.6948-2  
 H2O2 4.817-10 5.487-11 1.0770-9 1.227-10 1.2750-9 1.452-10 1.5230-9 1.735-10 1.8660-9 2.125-10  
 H2SO4 2.729-11 8.227-10 2.779-10 6.2400-9 4.472-10 9.3350-9 7.372-10 1.4200-8 1.2930-9 2.2660-8  
 NO 9.4443-5 1.4817-5 9.4442-5 1.4817-5 9.4442-5 1.4816-5 9.4441-5 1.4816-5 9.4441-5 1.4816-5  
 NO2 1.0011-6 5.1936-7 2.2385-6 1.1613-6 2.6487-6 1.3741-6 3.1657-6 1.6423-6 3.8772-6 2.0114-6  
 NO3 1.255-13 2.774-14 6.274-13 1.387-13 8.784-13 1.942-13 1.255-12 2.774-13 1.882-12 4.162-13  
 N2 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1  
 N2O 5.5982-9 1.0091-9 1.2518-8 2.2563-9 1.4811-8 2.6697-9 1.7703-8 3.1909-9 2.1681-8 3.9081-9  
 NA 2.980-12 3.457-17 3.465-13 1.695-18 1.956-13 9.138-19 1.035-13 4.773-19 4.910-14 2.296-19  
 NaOH 2.3040-8 1.082-11 8.9570-9 1.774-12 6.5080-9 1.231-12 4.5010-9 8.404-13 2.8930-9 5.479-13  
 Na2SO4 2.8500-9 6.157-11 4.3970-9 1.255-11 3.7280-9 9.043-12 2.9390-9 6.406-12 2.1290-9 4.346-12  
 O 3.4940-9 1.966-11 1.5630-9 8.794-12 1.3210-9 7.432-12 1.1050-9 6.216-12 9.022-10 5.077-12  
 OH 1.5471-6 5.5773-8 1.0346-6 3.7297-8 9.5112-7 3.4288-8 8.6998-7 3.1363-8 7.8611-7 2.8340-8  
 O2 6.6260-2 6.6300-2 6.6259-2 6.6299-2 6.6299-2 6.6259-2 6.6299-2 6.6257-2 6.6298-2  
 O3 1.882-12 9.757-14 4.208-12 2.226-13 4.977-12 2.634-13 5.751-12 3.148-13 7.298-12 3.856-13  
 SO2 3.6748-6 2.4552-6 3.3473-6 1.6655-6 3.2519-6 1.5043-6 3.1394-6 1.3400-6 2.9969-6 1.1639-6  
 SO3 3.0881-7 1.5160-6 6.2898-7 2.2996-7 7.2300-7 2.4575-6 8.3425-7 2.6165-6 9.7536-7 2.7834-6  
 M, MOLE WT 28.888 28.888 28.888 28.888 28.888 28.888 28.888 28.888 28.888 28.888  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

SOLUTION 2

NaOH(L) 1.9086-5 4.7472-7 3.7105-5 3.8912-7 3.7746-5 3.7806-7 3.7293-5 3.6860-7 3.5952-5 3.6048-7  
 Na2SO4(S) 0.000 0 5.011-12 0.000 0 2.284-12 0.000 0 1.947-12 0.000 0 1.649-12 0.000 0 1.370-12  
 Na2SO3(L) 1.553-10 0.000 0 5.345-10 0.000 0 5.374-10 0.000 0 5.064-10 0.000 0 4.493-10 0.000 0  
 Na2SO4(I) 0.000000 5.4922-1 0.000000 5.5976-1 0.000000 5.6464-1 0.000000 5.7146-1 0.000000 5.8145-1  
 Na2SO4(L) 4.2901-2 0.000000 3.3026-1 0.000000 3.9286-1 0.000000 4.4249-1 0.000000 4.8080-1 0.000000  
 Na2V2O6(L) 9.5365-1 4.4715-1 6.6773-1 4.1527-1 6.0557-1 3.9971-1 5.5618-1 3.7788-1 5.1785-1 3.4585-1  
 Na4V2O7(S) 3.0255-3 1.1437-5 1.6014-3 1.4272-6 3.1073-5 9.2623-7 6.7370-4 5.8267-7 3.8885-4 3.4003-7  
 Na6V2O8(S) 4.6751-8 0.000000 1.8705-8 0.000000 9.2689-9 0.000000 3.9746-9 0.000000 1.4204-9 0.000000  
 V2O3(S) 1.2550-9 5.388-11 2.326-10 7.447-11 2.038-10 7.594-11 1.918-10 7.553-11 1.921-10 7.227-11  
 V2O5(L) 4.0154-4 3.6135-3 3.7194-4 2.4974-2 4.5633-4 3.5652-2 6.1337-4 5.0653-2 9.2173-4 7.2705-2  
 M, MOLE WT 239.65 187.71 210.30 185.32 203.89 184.16 198.80 182.53 194.86 180.15  
 PHASE FRACTION 1.2851-8 2.7286-8 1.8366-8 2.7939-8 2.0260-8 2.8252-8 2.2064-8 2.8702-8 2.3692-8 2.9387-8  
 PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH2OH	CH3O	CH4	CH
CH	CH2	DIN	DOS	DS	CS2	C2	C2H	C2H2	C2
C2H4	C2H402	C2H404	C2H5	C2H6	CH3CH2CH3	C2H5OH	CH3COCH3	C2N	C2
C2D	C3	C3H60	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	C5	C6H5	C4H50	C4H6	C4H5OH	C7H8	C8
N-C8H18	I-C8H18	O-C12H27	C12H10	HDI	H2O	HCO	H2O2	H2S	N
NaO	Na2	Na2C2O4	Na2D	Na2D2H2	S	SH	SN	NaOH	Na
S2O	S8	V	VN	VO	VO2			S2	

SOLUTION 2

NaOH(A)	Na2O(C)	Na2O(A)	Na2O(L)	Na2SO4(IV)	Na2V2O6(S)	Na6V2O8(L)	V2O3(L)	V2O5(S)
PURE SPECIES								
C(GR)	C7H8(L)	CBH18(L)	K2O(S)	K2O(L)	K2O4(L)	W(S)	K2HSO4(S)	NA(S)
NaOH(S)	NaOH(L)	Na2O2(S)	Na2O3(I)	Na2O3(2)	Na2O3(L)	Na2O2(A)	Na2O2(B)	Na2S(I)
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	V0(S)
V02(S)	V02(S)	V02(L)						V0

CASE NO. 8701 312 0.01% SULFUR, 10 NA, 1.0 V PPM TIME = 0.673 SEC  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

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SOLUTION 1

AR 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3  
 CO 3.0980-9 9.534-12 1.3860-9 4.265-12 1.1710-9 3.504-12 9.777-10 3.015-12 8.000-10 2.462-12  
 CO2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2  
 H 5.874-12 4.834-15 1.757-12 1.446-15 1.365-12 1.123-15 1.045-12 8.596-16 7.707-13 6.342-16  
 HNO 1.515-12 1.651-14 2.285-12 2.449-14 2.444-12 2.588-14 2.694-12 2.938-14 2.981-12 3.250-14  
 HNO2 4.1198-9 1.6059-9 1.3775-8 5.3495-9 1.7729-8 6.9108-9 2.3167-8 9.0303-9 3.1400-8 1.2240-8  
 HNO3 1.205-11 1.509-11 9.011-11 1.128-10 1.372-10 1.718-10 2.143-10 2.683-10 3.558-10 4.454-10  
 HO2 1.1950-8 9.702-10 1.7870-8 1.4510-9 1.9440-8 1.5780-9 2.1250-8 1.7250-9 2.3520-8 1.9090-9  
 H2 2.6140-9 1.618-11 1.1690-9 7.234-12 9.881-10 6.114-12 8.267-10 5.116-12 6.750-10 4.177-12  
 H2O 9.6946-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2  
 H2O2 4.817-10 5.487-11 1.0770-9 1.227-10 1.2750-9 1.452-10 1.5230-9 1.735-10 1.8660-9 2.125-10  
 H2SO4 2.591-11 7.719-10 2.610-10 5.8550-9 4.199-10 8.7600-9 6.919-10 1.3320-8 1.2130-9 2.1260-8  
 NO 9.4444-5 1.4817-5 9.4443-5 1.4817-5 9.4442-5 1.4817-5 9.4442-5 1.4817-5 9.4442-5 1.4817-5  
 NO2 1.0011-6 5.1937-7 2.2386-6 1.1613-6 2.6487-6 1.3741-6 3.1658-6 1.5423-6 3.8772-6 2.0114-6  
 N2S 1.255-13 2.775-14 6.274-13 1.397-13 8.784-13 1.942-13 1.225-12 2.774-13 1.882-12 4.162-13  
 N2 7.3699-1 7.3703-1 7.3699-1 7.3704-1 7.3699-1 7.3704-1 7.3699-1 7.3704-1 7.3699-1 7.3704-1  
 N2O 5.5983-9 1.0091-9 1.2518-8 2.2564-9 1.4811-8 2.6698-9 1.7703-8 3.1910-9 2.1682-8 3.9081-9  
 NA 1.417-11 4.705-17 6.048-13 2.285-18 3.144-13 1.227-18 1.569-13 6.389-19 7.138-14 3.037-19  
 NAO 1.684-12 9.143-18 1.613-13 9.929-19 9.886-14 6.307-19 5.896-14 3.914-19 3.286-14 2.286-19  
 NAOH 1.0950-7 1.473-11 1.5680-8 2.392-12 1.0460-8 1.653-12 6.8190-9 1.121-12 4.2060-9 7.249-13  
 NA2SO4 6.1170-8 1.070-10 1.2640-8 2.141-11 9.0370-9 1.529-11 6.3310-9 1.071-11 4.2230-9 7.139-12  
 O 3.4940-9 1.966-11 1.5630-9 8.794-12 1.3210-9 7.452-12 1.1050-9 6.218-12 9.022-10 5.077-12  
 OH 1.5471-6 5.5773-8 1.0346-6 3.7297-8 9.5112-7 3.4288-8 8.6998-7 3.1363-8 7.8611-7 2.8340-8  
 O2 6.6261-2 6.6302-2 6.6260-2 6.6301-2 6.6260-2 6.6300-2 6.6259-2 6.6300-2 6.6258-2 6.6300-2  
 O3 1.882-12 9.957-14 4.208-12 2.226-13 4.979-12 2.634-13 5.951-12 3.149-13 7.289-12 3.856-13  
 SO2 3.4891-6 2.3036-6 3.1437-6 1.5628-6 3.0529-6 1.4115-6 2.9465-6 1.2574-6 2.8124-6 1.0922-6  
 SO3 2.9321-7 1.4224-6 5.9073-7 2.1577-6 6.7876-7 2.3059-6 7.8301-7 2.4532-6 9.1531-7 2.6120-6  
 M, MOLE WT 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

SOLUTION 2

NAOH(L) 9.0749-5 6.4621-7 6.4974-5 5.2469-7 6.0452-5 5.0755-7 5.5497-5 4.9190-7 5.2269-5 4.7693-7  
 NA2O(C) 1.693-11 0.000 0 1.736-12 0.000 0 1.081-12 0.000 0 0.000 0 0.000 0 0.000 0  
 NA2SO3(S) 0.000 0 8.712-12 0.000 0 3.896-12 0.000 0 3.293-12 0.000 0 2.755-12 0.000 0 2.250-12  
 NA2SO3(L) 3.3330-9 0.000 0 1.5330-9 0.000 0 1.3030-9 0.000 0 1.0910-9 0.000 0 8.913-10 0.000 0  
 NA2SO4(I) 0.000000 9.5486-1 0.000000 9.5493-1 0.000000 9.5496-1 0.000000 9.5501-1 0.000000 9.5509-1  
 NA2SO4(L) 9.2095-1 0.000000 9.5112-1 0.000000 9.5231-1 0.000000 9.5314-1 0.000000 9.5375-1 0.000000  
 NA2V2O6(L) 7.3670-2 4.4942-2 4.8446-2 4.3625-2 4.7400-2 4.2913-2 4.6654-2 4.1840-2 4.6091-2 4.0099-2  
 NA4V2O7(S) 5.2843-3 2.1299-6 3.5627-4 2.7260-7 2.1696-4 1.7923-7 1.2969-4 1.1490-7 7.3118-5 6.9007-8  
 NA6V2O8(S) 1.8460-6 0.000 0 1.2760-8 0.000 0 4.8370-9 0.000 0 1.7560-9 0.000 0 5.450-10 0.000 0  
 V2O3(S) 4.290-12 2.922-12 5.503-12 4.303-12 6.179-12 4.523-12 7.010-12 4.696-12 8.090-12 4.787-12  
 V2O5(L) 1.3720-6 1.9600-4 8.8003-6 1.4430-3 1.3833-5 2.1236-3 2.2419-5 3.1492-3 3.8811-5 4.8157-3  
 M, MOLE WT 150.40 146.62 147.02 146.54 146.89 146.49 146.80 146.42 146.74 146.31  
 PHASE FRACTION 1.5579-7 2.7248-7 2.5199-7 2.7291-7 2.5823-7 2.7311-7 2.6278-7 2.7339-7 2.6621-7 2.7385-7

PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH20H	CH30	CH4	CH
CN	CH2	CNH	COS	CS	CS2	C2	C2H	C2K2	C2
C2H4	C2H402	C2H404	C2H5	C2H6	C2H3C2H3	C2H5OH	C2H3C2H3	C2N	C2
C2O	C3	C3H6	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	CS	C4H5	C4H50	C4H6	C4H5OH	C7H8	C8
N-C8H18	I-C8H18	O-C12H9	C12H10	HCO	HCO2	H2O2	H2S	N	
NO	NH	NH2	NH3	N2H4	N2O4	N2O5	N3	NHON	NA
NA2	NA2C2H2	NA2D	NA2O2H2	S	SH	SN	SO	S2	S2

SB	V	VH	VO	VO2					
SOLUTION 2									
NAOH(A)	NA2O(A)	NA2O(L)	NA2SO4(IV)	NA2V2O6(S)	NA6V2O8(L)	V2O3(L)	V2O5(L)		
PURE SPECIES									
C(6R)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	NA2HSO4(S)	NA1(S)	NA
NAON(L)	NAON(L)	NAO2(S)	NA2O3(I)	NA2O3(2)	NA2O3(L)	NA2O2(A)	NA2O2(B)	NA2S(I)	NA
NA2S(L)	S(S)	S(L)	V(S)	V(L)	NAV3O8(S)	NA2V12O31(S)	NA2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

CASE NO. 8701 113 0.011SULFUR, 0.1 NA, 10. V PPM TIME = 0.483 SEC  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

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SOLUTION 1

AR 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3  
 CO 3.0980-9 9.536-12 1.3860-9 4.265-12 1.1710-9 3.504-12 9.797-10 3.015-12 8.000-10 2.482-12  
 CO2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2  
 H 5.874-12 4.834-15 1.757-12 1.446-15 1.345-12 1.123-15 1.045-12 8.596-16 7.707-13 6.342-16  
 HO 1.515-12 1.651-14 2.255-12 2.469-14 2.454-12 2.686-14 2.694-12 2.936-14 2.981-12 3.250-14  
 HO2 4.1198-9 1.6059-9 1.3775-8 5.3494-9 1.7729-8 6.9107-9 2.3167-8 9.0302-9 3.1400-8 1.2240-8  
 HO3 1.205-11 1.509-11 9.011-11 1.128-10 1.372-10 1.718-10 2.143-10 2.683-10 3.558-10 4.454-10  
 H2O 1.1950-8 9.702-10 1.7870-8 4.1510-9 1.9440-8 1.5780-9 2.1250-9 1.7250-9 2.3520-8 1.9090-9  
 H2 2.6140-9 1.618-11 1.1690-9 7.235-12 9.881-10 6.114-12 8.267-10 5.116-12 6.750-10 4.177-12  
 H2O 7.6946-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2  
 H2O2 4.817-10 5.487-11 1.0770-9 1.227-10 1.2750-9 1.452-10 1.5230-9 1.735-10 1.8860-9 2.125-10  
 H2SO4 2.731-11 8.258-10 2.786-10 6.2640-9 4.486-10 9.3730-9 7.396-10 1.4260-8 1.2970-9 2.2750-8  
 NO 9.4444-5 1.4817-5 9.4443-5 1.4817-5 9.4442-5 1.4817-5 9.4442-5 1.4817-5 9.4441-5 1.4816-5  
 NO2 1.0011-6 5.1936-7 2.2386-6 1.1613-6 2.6487-6 1.3741-6 3.1658-6 1.6423-6 3.8772-6 2.0114-6  
 N03 1.255-13 2.775-14 6.274-13 1.387-13 8.784-13 1.942-13 1.255-12 2.774-13 1.882-12 4.162-13  
 N2 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1  
 N2O 5.5983-9 1.0091-9 1.2518-8 2.2564-9 1.4811-8 2.6698-9 1.7703-8 3.1910-9 2.1682-8 3.9081-9  
 NaOH 7.068-11 1.461-13 3.172-11 6.437-14 2.682-11 5.395-14 2.245-11 4.456-14 1.833-11 3.560-14  
 O 3.4940-9 1.966-9 1.5630-9 8.794-12 1.3210-9 7.432-12 1.1050-9 6.218-12 9.022-10 5.077-12  
 OH 1.5471-6 5.5773-8 1.0346-6 3.7297-8 9.5112-7 3.4288-8 8.6998-7 3.1363-8 7.8611-7 2.8340-8  
 O2 6.6261-2 6.6301-2 6.6260-2 6.6300-2 6.6260-2 6.6259-2 6.6300-2 6.6259-2 6.6299-2  
 O3 1.882-12 9.757-14 4.206-12 2.226-13 4.979-12 2.634-13 5.951-12 3.149-13 7.289-12 3.856-13  
 SO2 3.6779-6 2.4644-6 3.3561-6 1.6721-6 3.2614-6 1.5103-6 3.1494-6 1.3454-6 3.0071-6 1.1688-6  
 SO3 3.0907-7 1.5217-6 6.3063-7 2.3086-6 7.2513-7 2.4673-6 8.3491-7 2.6271-6 9.7867-7 2.7952-6  
 M, MOLE WT 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

SOLUTION 2

NaOH(L) 5.8561-8 6.4091-9 1.3142-7 1.4117-8 1.5556-7 1.6564-8 1.8599-7 1.9544-8 2.2783-7 2.3422-8  
 Na2SO4(I) 0.000000 1.0049-4 0.000000 7.3965-4 0.000000 1.0892-3 0.000000 1.6131-3 0.000000 2.4451-3  
 Na2SO4(L) 4.0424-7 0.000000 4.1539-6 0.000000 6.6972-6 0.000000 1.1041-5 0.000000 1.9374-5 0.000000  
 Na2V2O6(L) 2.1871-2 2.2056-2 2.2025-2 2.1402-2 2.2042-2 2.1046-2 2.2056-2 2.0509-2 2.2064-2 1.9639-2  
 Na4V2O7(S) 6.533-10 1.029-10 6.626-10 9.682-11 6.637-10 9.362-11 6.645-10 8.891-11 6.650-10 8.152-11  
 V2O3(S) 3.0580-6 1.4580-6 6.1150-7 2.9160-9 4.3680-7 2.0830-9 3.0580-7 1.4580-9 2.0380-7 9.721-10  
 V2O5(L) 9.7813-1 9.7784-1 9.7797-1 9.7786-1 9.7787-1 9.7795-1 9.7788-1 9.7792-1 9.7790-1  
 M, MOLE WT 183.24 183.24 183.24 183.18 183.25 183.14 183.25 183.25 183.09 183.25 183.00  
 PHASE FRACTION 1.2300-7 1.2301-7 1.2300-7 1.2309-7 1.2300-7 1.2313-7 1.2300-7 1.2320-7 1.2300-7 1.2330-7

PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH2OH	CH3O	CH4	CH
CH	CH2	CHN	CO	CS	CS2	C2	C2H	C2H2	C2
C2H4	C2H402	C2H404	C2H5	C2H6	C3H32CH3	C2H5OH	C3H3OCH3	C2N	C2
C2D	C3	C3H60	N-C3H7	I-C3H7	C3H8	1-C3H7OH	C3O2	C4	C4
M-C4H10	I-C4H10	C4H2	CS	C4H5	C4H5O	C4H6	C4H5OH	C7H8	C8
M-C5H12	I-C5H12	O-C12H9	C12H10	HCO	HCO	HCO	H2O2	H2S	N
NCO	NH	NH2	NH3	N2H4	N2O4	N2O5	N3	NA	NA
NAH	NA0	NA2	NA2C2H2	NA2D	NA2O2H2	NA2SO4	S	SH	SN
SO	S2	S20	S8	V	VN	VO	VO2		

SOLUTION 2

NaOH(A) Na2D(C) Na2D(L) Na2SO3(S) Na2SO3(L) Na2SO4(IV) Na2V2O6(S) Na6V2O8(S) NA

V2O3(L) V2O5(S)

PURE SPECIES

C(6R)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	N2H5SO4(S)	NA(S)	NA
NaOH(S)	NaOH(L)	Na2O(S)	Na2O(L)	Na2O3(S)	Na2O3(L)	Na2O2(A)	Na2O2(B)	Na2S(1)	NA

NA2S(L)	S(S)	S(L)	V(S)	V(L)	NAV3OB(S)	NA2V12O31(S)	NA2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

CASE NO. 8701 213 0.01% SULFUR, 1.0 NA, 10 V PPM TIME = 0.508 SEC  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0  
 SOLUTION 1  
 AR 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3  
 CO 3.0980-9 9.536-12 1.3860-9 4.265-12 1.1710-9 3.604-12 9.797-10 3.015-12 8.000-10 2.442-12  
 CO2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2 9.0897-2  
 H 5.874-12 4.834-15 1.757-12 1.446-15 1.365-12 1.123-15 1.045-12 8.596-16 7.707-13 6.342-16  
 HNO 1.515-12 1.651-14 2.265-12 2.464-14 2.686-14 2.694-12 2.936-14 2.981-12 3.250-14  
 HNO2 4.1198-9 1.6059-9 1.3775-8 5.3695-9 1.7729-8 6.9107-9 2.3167-8 9.0302-9 3.1400-8 1.2240-8  
 HNO3 1.205-11 1.509-11 9.011-11 1.128-10 1.372-10 1.718-10 2.143-10 2.683-10 3.558-10 4.454-10  
 H2O 1.1950-8 9.702-10 1.7870-8 1.4510-9 1.9440-8 1.5780-9 2.1250-8 1.7250-9 2.3520-8 1.9090-9  
 H2 2.6140-9 1.618-11 1.1690-9 7.234-12 9.881-10 6.114-12 8.267-10 5.116-12 6.750-10 4.177-12  
 H2O 9.6946-2 9.6947-2 9.6946-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2 9.6947-2  
 H2O2 4.817-10 5.487-11 1.0770-9 1.227-10 1.2750-9 1.452-10 1.5230-9 1.735-10 1.8660-9 2.125-10  
 H2SO4 2.731-11 8.259-10 2.786-10 6.2630-9 4.486-10 9.3690-9 7.396-10 1.4250-8 1.2970-9 2.2730-8  
 NO 9.4444-5 1.4817-5 9.4443-5 1.4817-5 9.4442-5 1.4817-5 9.4442-5 1.4817-5 9.4441-5 1.4817-5  
 NO2 1.0011-6 5.1937-7 2.2386-6 1.1613-6 2.6487-6 1.3741-6 3.1650-6 1.6423-6 3.8772-6 2.0114-6  
 N2O 1.255-13 2.775-14 6.274-13 1.387-13 8.784-13 1.942-13 1.255-12 2.774-13 1.882-12 4.162-13  
 N2 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1 7.3699-1 7.3703-1  
 N2O 5.5983-9 1.0091-9 1.2518-8 2.2564-9 1.4811-8 2.6698-9 1.7703-8 3.1910-9 2.1682-8 3.9081-9  
 NaOH 2.514-10 5.172-13 1.126-10 2.259-13 9.519-11 1.885-13 7.965-11 1.547-13 6.502-11 1.223-13  
 Na2SO4 3.398-13 1.411-13 6.954-13 2.043-13 7.998-13 2.127-13 9.232-13 2.178-13 1.079-12 2.173-13  
 O 3.4940-9 1.966-11 1.5630-9 8.794-12 1.3210-9 7.432-12 1.1050-9 6.218-12 9.022-10 5.077-12  
 OH 1.5471-6 5.5773-8 1.0346-6 3.7297-8 9.5112-7 3.4288-8 8.8998-7 3.1363-8 7.8611-7 2.8340-8  
 O2 6.6261-2 6.6301-2 6.6260-2 6.6300-2 6.6260-2 6.6300-2 6.6259-2 6.6300-2 6.6258-2 6.6279-2  
 O3 1.882-12 9.957-14 4.208-12 2.226-13 4.979-12 2.634-13 5.951-12 3.149-13 7.288-12 3.856-13  
 SO2 3.6779-6 2.4644-6 3.3561-6 1.6716-6 3.2614-6 1.5057-6 3.1494-6 1.3447-6 3.0070-6 1.1678-6  
 SO3 3.0907-7 1.5217-6 6.3063-7 2.3080-6 7.2513-7 2.4663-6 8.3691-7 2.6256-6 9.7867-7 2.7928-6  
 M, MOLE WT 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0  
 SOLUTION 2  
 NaOH(L) 2.0832-7 2.2685-8 4.6653-7 4.9553-8 5.5207-7 5.7883-8 6.5986-7 6.7848-8 8.0804-7 8.0474-8  
 Na2SO4(II) 0.000000 1.2589-3 0.000000 9.1107-3 0.000000 1.3284-2 0.000000 1.9430-2 0.000000 2.9075-2  
 Na2SO4(L) 5.1158-6 0.000000 5.2348-5 0.000000 8.4288-5 0.000000 1.3898-4 0.000000 2.4370-4 0.000000  
 Na2SO4(L) 5.1158-6 0.000000 5.2348-5 0.000000 8.4288-5 0.000000 1.3898-4 0.000000 2.4370-4 0.000000  
 Na2V2O6(L) 2.2055-1 2.2005-1 2.2106-1 2.1045-1 2.2109-1 2.0536-1 2.2109-1 1.9785-1 2.2101-1 1.8607-1  
 Na4V2O7(S) 8.3369-8 1.2852-8 8.3812-8 1.1730-8 8.3943-8 1.1155-8 8.3946-8 1.0336-8 8.3790-8 9.1171-7  
 V2O3(S) 2.4370-6 1.1610-8 4.8710-7 2.3270-9 3.4790-7 1.6640-9 2.4350-7 1.1670-9 1.6230-7 7.802-10  
 V2O5(L) 7.7944-1 7.7870-1 7.7889-1 7.8044-1 7.7882-1 7.8136-1 7.7877-1 7.8272-1 7.7874-1 7.8486-1  
 M, MOLE WT 195.55 195.47 195.58 194.56 195.58 194.08 195.58 193.37 195.57 192.25  
 PHASE FRACTION 1.2300-7 1.2315-7 1.2300-7 1.2413-7 1.2301-7 1.2465-7 1.2301-7 1.2343-7 1.2303-7 1.2668-7  
 PURE SPECIES PHASE FRACTIONS (IF ANY)  
 ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS  
 SOLUTION 1  
 C CH CH2 CH2O CH2O2 CH3 CH2OH CH3O CH4 CH  
 CN CH2 CN CH3S CS CS2 C2 C2H C2H2 C2  
 C2H4 C2H4O2 C2H4O4 C2H5 C2H6 CH3NCH3 C2H5OH C3OCH3 C2N C2  
 C2O C3 C3H60 N-C3H7 I-C3H7 C3H8 1-C3H7OH C3O2 C4 C4  
 N-C4H10 I-C4H10 C4H2 C5 C4H5 C4H50 C4H6 C4H5OH C7H8 C8  
 N-C8H18 I-C8H18 O-C12H9 C12H10 HCN HCO HCO2 H2N2 N  
 NCO NH NH2 NH3 N2H4 N2O4 N2O5 N3 NA NA  
 NAH NAO NAO NAO NAO NAO NAO NAO N  
 S2 S2O S8 V VN VO VO2 SH SN SN SO  
 SOLUTION 2  
 NaOH(A) Na2O(C) Na2O(A) Na2O(L) Na2SO3(S) Na2SO3(L) Na2SO4(IV) Na2V2O6(S) Na4V2O8(S) NA  
 V2O3(L) V2O5(S)  
 PURE SPECIES

C(GR)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	N2H8SO4(S)	NA(S)	NA
NaOH(S)	NaOH(L)	NaO2(S)	Na2O3(S)	Na2O3(S)	Na2O3(L)	Na2O2(A)	Na2O2(B)	Na2S(1)	NA
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

CASE NO. 8701 313 0.017SULFUR, 10 NA, 10. V PPM TIME = 0.677 SEC  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

## SOLUTION 1

AR 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3 8.8006-3  
 CO 3.0890-9 9.535-12 1.3860-9 4.264-12 1.1710-9 3.604-12 9.797-10 3.015-12 7.999-10 2.462-12  
 CO2 9.0896-2 9.0896-2 9.0896-2 9.0896-2 9.0896-2 9.0896-2 9.0896-2 9.0896-2 9.0896-2 9.0896-2  
 H 5.874-12 4.854-15 1.757-12 1.446-15 1.345-12 1.123-15 1.045-12 8.596-16 7.707-13 6.342-16  
 HNO 1.515-12 1.651-14 2.265-12 2.469-14 2.464-12 2.686-14 2.694-12 2.936-14 2.981-12 3.250-14  
 HNO2 4.1198-9 1.6059-9 1.3775-8 5.3695-9 1.7729-8 6.9108-9 2.3167-8 9.0303-9 3.1400-8 1.2240-8  
 HNO3 1.205-11 1.509-11 9.011-11 1.128-10 1.372-10 1.718-10 2.143-10 2.683-10 3.558-10 4.454-10  
 HO 1.1950-8 9.702-10 1.7870-8 1.4510-9 1.9440-8 1.5780-9 2.1250-8 1.7250-9 2.3520-8 1.9090-9  
 H2 2.6140-9 1.618-11 1.1690-9 7.234-12 9.881-10 6.114-12 8.267-10 5.116-12 6.750-10 4.177-12  
 H2O 9.6945-2 9.6946-2 9.6946-2 9.6946-2 9.6946-2 9.6946-2 9.6946-2 9.6946-2 9.6946-2 9.6946-2  
 H2O2 4.817-10 5.487-11 1.0770-9 1.227-10 1.2750-9 1.452-10 1.5230-9 1.735-10 1.8660-9 2.125-10  
 H2SO4 2.656-11 7.946-10 2.686-10 6.0190-9 4.322-10 8.9980-9 7.123-10 1.3670-8 1.2490-9 2.1780-8  
 NO 9.4444-5 1.4817-5 9.4443-5 1.4817-5 9.4443-5 1.4817-5 9.4443-5 1.4817-5 9.4442-5 1.4817-5  
 NO2 1.0012-6 5.1937-7 2.2386-6 1.1613-6 2.6487-6 1.3741-6 3.1658-6 1.6424-6 3.8773-6 2.0115-6  
 NO3 1.255-13 2.775-14 6.274-13 1.387-13 8.784-13 1.942-13 1.255-12 2.775-13 1.882-12 4.162-13  
 N2 7.3699-1 7.3704-1 7.3699-1 7.3704-1 7.3699-1 7.3704-1 7.3699-1 7.3704-1 7.3699-1 7.3704-1  
 N2O 5.5983-9 1.0091-9 1.2518-8 2.2564-9 1.4812-8 2.6698-9 1.7703-8 3.1910-9 2.1682-8 3.9081-9  
 NA 9.265-12 3.520-17 4.447-13 1.725-18 2.318-13 9.304-19 1.162-13 4.861-19 5.304-14 2.340-19  
 NAO 1.101-12 6.840-18 1.182-13 7.497-19 7.290-14 4.784-19 4.367-14 2.987-19 2.442-14 1.761-19  
 NAOH 7.1620-8 1.102-11 1.1490-8 1.804-12 7.7120-9 1.254-12 5.0500-9 8.559-13 3.1250-9 5.584-13  
 NA2SO4 2.6810-8 6.168-11 6.9840-9 1.255-11 5.0580-9 9.037-12 3.5750-9 6.400-12 2.4010-9 4.339-12  
 O 3.4940-9 1.966-11 1.5630-9 8.794-12 1.3210-9 7.432-12 1.1050-9 6.218-12 9.022-10 5.077-12  
 OH 1.5471-6 5.5773-8 1.0346-6 3.7297-8 9.5112-7 3.4288-8 8.6998-7 3.1363-8 7.8611-7 2.8340-8  
 O2 6.6262-2 6.6302-2 6.6261-2 6.6302-2 6.6261-2 6.6260-2 6.6301-2 6.6259-2 6.6300-2  
 O3 1.882-12 9.957-14 4.208-12 2.226-13 4.979-12 2.634-13 5.9512-12 3.149-13 7.289-12 3.856-13  
 SO2 3.5763-6 2.3714-6 3.2354-6 1.6065-6 3.1424-6 1.4499-6 3.0333-6 1.2903-6 2.8954-6 1.1190-6  
 SO3 3.0054-7 1.4643-6 6.0796-7 2.2182-6 6.9867-7 2.3888-6 8.0606-7 2.5194-6 9.4233-7 2.6760-6  
 M, MOLE WT 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868 28.868  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

## SOLUTION 2

NAOH(L) 5.9341-5 4.8344-7 4.7617-5 3.9614-7 4.4723-5 3.8494-7 4.1841-5 3.7543-7 3.8839-5 3.6736-7  
 NA2O(C) 7.241-12 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0  
 NA2SO3(S) 0.000 0 5.019-12 0.000 0 2.283-12 0.000 0 1.946-12 0.000 0 1.647-12 0.000 0 1.368-12  
 NA2SO3(L) 1.4610-9 0.000 0 8.509-10 0.000 0 7.291-10 0.000 0 6.160-10 0.000 0 5.066-10 0.000 0  
 NA2SO4(I) 0.000000 5.5016-1 0.000000 5.5958-1 0.000000 5.6426-1 0.000000 5.7085-1 0.000000 5.8056-1  
 NA2SO4(L) 4.0363-1 0.000000 5.2574-1 0.000000 5.3299-1 0.000000 5.3820-1 0.000000 5.4215-1 0.000000  
 NA2V2O6(L) 5.7854-1 4.4635-1 4.7218-1 4.1826-1 4.6556-1 4.0122-1 4.6045-1 3.8004-1 4.5672-1 3.4883-1  
 NA4V2O7(S) 1.7744-2 1.1839-5 1.8650-3 1.4827-6 1.1587-3 9.6391-7 7.0240-4 6.0792-7 4.0005-4 3.5619-7  
 NA6V2O8(S) 2.6506-6 0.000000 3.5878-8 0.000000 1.4045-8 0.000000 5.2165-9 0.000000 1.7067-9 0.000000  
 V2O3(S) 7.878-11 5.186-11 9.986-11 7.203-11 1.116-10 7.352-11 1.262-10 7.322-11 1.452-10 7.019-11  
 V2O5(L) 2.5198-5 3.4781-3 1.5970-4 2.4154-2 2.4989-4 3.4517-2 4.0357-4 4.9105-2 6.9653-4 7.0609-2  
 M, MOLE WT 203.85 187.63 190.42 185.38 189.64 184.27 189.07 182.69 188.63 180.37  
 PHASE FRACTION 2.0626-7 2.7342-7 2.5937-7 2.7927-7 2.6339-7 2.8227-7 2.6636-7 2.8661-7 2.6866-7 2.9324-7

## PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

## SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH20H	CH30	CH4	CH
CN	CN2	CNN	COS	CS	CS2	C2	C2H	C2H2	C2
C2H4	C2H4O2	C2H4O4	C2H5	C2H6	C2H5C2H3	C2H5OH	C2H5OCH3	C2N	C2
C2O	C3	C3H6O	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	C5	C6H5	C6H5O	C6H6	C6H5OH	C7H8	C8
N-C8H18	I-C8H18	O-C12H27	C12H10	HCO	HCO	H2N2	H2S	N	
N2O	NH	NH2	NH3	N2H4	N2O4	N2O5	N3	N4O	NA
N4	N4C2N2	NA2O	NA2O2H2	S	SH	SN	SO	S2	S2

## SOLUTION 2

NaOH(A)	Na2O(A)	Na2O(L)	Na2SO4(IV)	Na2V2O6(S)	Na6V2O8(L)	V2O3(L)	V2O5(S)		
PURE SPECIES									
C(SR)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	N2H8SO4(S)	NA(S)	NA
NaOH(S)	NaOH(L)	NaO2(S)	Na2CO3(1)	Na2CO3(2)	Na2CO3(L)	Na2O2(A)	Na2O2(B)	Na2S(1)	NA
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

STOP

## SOLN 1 GASES

SOLN 2	V205(L)	V203(L)	V204(L)	VCL4(L)
SOLN 2	NA2SO3(L)	NA2SO4(L)	NAOH(L)	
SOLN 2	NA2O(L)	NA2V206(S)	NA4V207(S)	NA6V208(S)

CASE NO. 8701 121 0.1% SULFUR, 0.1 NA, 0.1 V PPM singular matrix, iteration 40 variable 7  
 P, ATM 1.0000 1.0000 7.0000 7.0000  
 T, DEG K 1172.0 977.0 1172.0 977.0

## SOLUTION 1

AR	8.8009-3	8.8009-3	8.8009-3	8.8010-3
CO	3.0930-9	9.522-12	1.1690-9	3.599-12
CO2	9.0819-2	9.0819-2	9.0819-2	9.0819-2
H	5.870-12	4.831-15	1.364-12	1.123-15
HNO	1.515-12	1.651-14	2.464-12	2.686-14
HNO2	4.1223-9	1.6068-9	1.7740-8	6.9143-9
HNO3	1.207-11	1.511-11	1.374-10	1.720-10
H2	1.1960-8	9.707-10	1.9450-8	1.5790-9
H2	2.6110-9	1.616-11	9.868-10	6.106-12
H2O	9.6876-2	9.6877-2	9.6876-2	9.6879-2
H2O2	4.817-10	5.487-11	1.2740-9	1.452-10
H2SO4	2.729-10	8.2480-9	4.4810-9	9.3600-8
NO	9.4506-5	1.4826-5	9.4503-5	1.4825-5
NO2	1.0024-6	5.2000-7	2.6521-6	1.3757-6
N2	7.3702-1	7.3707-1	7.3702-1	7.3707-1
N2O	5.6021-9	1.0097-9	1.4821-8	2.6714-9
NAOH	2.4320-9	3.428-12	1.0090-9	4.083-13
NA2SO4	3.181-10	6.203-11	8.994-10	9.984-12
O	3.4960-9	1.968-11	1.3210-9	7.437-12
OH	1.5470-6	5.5769-8	9.5107-7	3.4286-8
O2	6.6346-2	6.6381-2	6.6343-2	6.6376-2
O3	1.885-12	9.975-14	4.988-12	2.639-13
SO2	3.6745-5	2.4617-5	3.2582-5	1.5084-5
SO3	3.0899-6	1.5209-5	7.2485-6	2.4656-5
M, MOL WT	28.869	28.869	28.869	28.869

PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0

## SOLUTION 2

NAOH(L)	2.0152-6	1.5037-7	5.8532-6	1.2337-7
NA2SO3(S)	0.000	0	5.045-12	0.000
NA2SO3(L)	1.732-11	0.000	0	1.296-10
NA2SO4(I)	0.000000	5.5327-1	0.000000	6.2341-1
NA2SO4(L)	4.7891-3	0.000000	9.4780-2	0.000000
NA2V206(L)	9.5899-1	4.1345-1	8.7769-1	2.0800-1
NA4V207(S)	3.3944-5	1.0618-6	3.77441-5	5.3040-8
NA6V208(S)	5.852-12	0.000	0	7.779-12
V203(S)	1.1300-7	4.955-10	1.2260-8	3.587-10
V205(L)	3.6192-2	3.3275-2	2.7485-2	1.6859-1
M, MOL WT	241.13	185.46	232.51	169.93

PHASE FRACTION 1.2360-9 2.7534-9 1.3588-9 3.2663-9

## PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

## SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH2OH	CH3O	CH4	CH
CH	CH2	CHN	COS	CS	CS2	C2	C2H	C2H2	C2
C2H4	C2H4O2	C2H4O4	C2H5	C2H6	C2H3C2H3	C2H5OH	C2H3C2H3	C2N	C2
C2O	C3	C3H6O	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4

N-C4H10	I-C4H10	CAN2	C5	C6H5	C6H5O	C6H6	C6H5OH	C7H8	C8
N-C8H18	I-C8H18	O-C12H9	C12H10	HCO	HCO	H2O2	H2S	N	N
HCO	NH	NH2	NH3	NO3	NO2H	NO24	NO25	N3	NA
NAOH	NAH	NAO	NA2	NA2C2H2	NA2O	NA2O2H2	S	SH	SN
SO	S2	S2O	S8	V	VN	VO	VO2		

SOLUTION 2

NAOH(A)	NA2O(C)	NA2O(A)	NA2O(L)	NA2SO4(IV)	NA2V206(S)	NA6V208(L)	V203(L)	V205(S)	
PURE SPECIES									
C16R	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	N2H8SO4(S)	NA(S)	NA
NAOH(S)	NAOH(L)	NAO2(S)	NA2O3(1)	NA2O3(2)	NA2O3(L)	NA2O2(A)	NA2O2(B)	NA2S(I)	NA
NA2S(L)	S(S)	S(L)	V(S)	V(L)	NA2V203(S)	NA2V12031(S)	NA2V12031(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

CASE NO. 8701 221 0.17 SULFUR, 1.0 NA, 0.1 V PPM TIME = 0.611 SEC  
 P, ATM 1.0000 1.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

## SOLUTION 1

AR 8.8009-3 8.8009-3 8.8009-3 8.8010-3 8.8009-3 8.8010-3 8.8009-3 8.8010-3  
 CO 3.0930-9 9.522-12 1.1690-9 3.599-12 9.783-10 3.011-12 7.988-10 2.459-12  
 CO2 9.0818-2 9.0819-2 9.0819-2 9.0819-2 9.0819-2 9.0819-2 9.0819-2 9.0820-2  
 H 5.870-12 4.831-15 1.364-12 1.123-15 1.044-12 8.591-16 7.702-13 6.338-16  
 HNO 1.515-12 1.651-14 2.464-12 2.686-14 2.694-12 2.936-14 2.981-12 3.249-14  
 HNO2 4.1223-9 1.6068-9 1.7740-8 6.9143-9 2.3180-8 9.0349-9 3.1418-8 1.2246-8  
 HNO3 1.207-11 1.511-11 1.374-10 1.720-10 2.146-10 2.686-10 3.562-10 4.459-10  
 H2O 1.1960-8 9.707-10 1.9450-8 1.5790-9 2.1260-8 1.7260-9 2.3530-8 1.9100-9  
 H2 2.6110-9 1.616-11 9.868-10 6.104-12 8.256-10 5.109-12 6.741-10 4.172-12  
 H2O 9.6876-2 9.6877-2 9.6876-2 9.6878-2 9.6877-2 9.6878-2 9.6877-2 9.6878-2  
 H2O2 4.817-10 5.487-11 1.2740-9 1.452-10 1.5230-9 1.735-10 1.8850-9 2.125-10  
 H2SO4 2.777-10 8.2430-9 4.4780-9 9.3540-8 7.3830-9 1.4230-7 1.2950-8 2.2710-7  
 NO 9.4506-5 1.4826-5 9.4503-5 1.4825-5 9.4503-5 1.4825-5 9.4502-5 1.4825-5  
 NO2 1.0024-6 5.2000-7 2.6521-6 1.3757-6 3.1698-6 1.6442-6 3.8821-6 2.0137-6  
 NO3 1.257-13 2.780-14 8.801-13 1.946-13 1.257-12 2.779-13 1.886-12 4.169-13  
 N2 7.3702-1 7.3707-1 7.3702-1 7.3707-1 7.3702-1 7.3707-1 7.3702-1 7.3707-1  
 N2O 5.6021-9 1.0097-9 1.4821-8 2.6714-9 1.7715-8 3.1929-9 2.1696-8 3.9105-9  
 NA 2.285-12 1.439-17 9.491-14 3.753-19 4.762-14 1.949-19 2.174-14 9.293-20  
 NaOH 1.7670-8 4.505-12 3.1570-9 5.057-13 2.0700-9 3.431-13 1.2810-9 2.218-13  
 Na2SO4 1.6770-8 1.070-10 8.7980-9 1.530-11 6.2340-9 1.071-11 4.1850-9 7.145-12  
 O 3.4960-9 1.968-11 1.3210-9 7.437-12 1.1060-9 6.222-12 9.027-10 5.080-12  
 OH 1.5470-6 5.5769-8 9.5107-7 3.4286-8 8.6994-7 3.1361-8 7.8607-7 2.8337-8  
 O2 6.6346-2 6.6381-2 6.6343-2 6.6376-2 6.6342-2 6.6375-2 6.6340-2 6.6374-2  
 O3 1.885-12 9.975-14 4.988-12 2.639-13 5.962-12 3.154-13 7.302-12 3.863-13  
 SO2 3.6729-5 2.4601-5 3.2362-5 1.5075-5 3.1443-5 1.3430-5 3.0021-5 1.1667-5  
 SO3 3.0885-6 1.5200-5 7.2443-6 2.4641-5 8.3607-6 2.6238-5 9.7766-6 2.7916-5  
 M, MOLE WT 28.869 28.869 28.869 28.869 28.869 28.869 28.869 28.869  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

## SOLUTION 2

NaOH(L) 1.4636-5 1.9760-7 1.8312-5 1.5526-7 1.7149-5 1.5048-7 1.5916-5 1.4590-7  
 Na2SO3(S) 0.000 0 8.706-12 0.000 0 3.293-12 0.000 0 2.736-12 0.000 0 2.251-12  
 Na2SO3(L) 9.134-10 0.000 0 1.2670-9 0.000 0 1.0730-9 0.000 0 8.827-10 0.000 0  
 Na2SO4(I) 0.00000 9.5478-1 0.000000 9.5554-1 0.000000 9.5574-1 0.000000 9.5598-1  
 Na2SO4(L) 2.5253-1 0.000000 9.2712-1 0.000000 9.3846-1 0.000000 9.4517-1 0.000000  
 Na2V2O6(L) 7.4553-1 4.3206-2 7.2595-2 2.9088-2 6.1188-2 2.4537-2 5.4312-2 1.9289-2  
 Na4V2O7(S) 1.3921-3 1.9160-7 3.0311-5 1.1576-8 1.5685-5 6.3100-9 7.9940-6 3.1090-9  
 Na6V2O8(S) 1.2660-8 0.000 0 6.164-11 0.000 0 1.958-11 0.000 0 5.731-12 0.000 0  
 V2O3(S) 1.6650-9 2.999-11 1.036-10 3.271-11 9.958-11 2.937-11 1.026-10 2.456-11  
 V2O5(L) 5.3336-4 2.0138-3 2.3226-4 1.5373-2 3.1887-4 1.9721-2 4.9292-4 2.4736-2  
 M, MOLE WT 218.20 146.52 149.44 145.61 148.28 145.32 147.59 144.99  
 PHASE FRACTION 1.6456-9 2.7201-8 1.6683-8 2.7666-8 1.9993-8 2.7793-8 2.2441-8 2.7940-8

## PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.1000E-11 FOR ALL ASSIGNED CONDITIONS

## SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH2OH	CH3O	CH4	CH
CN	CH2	CHN	COS	CS	CS2	C2	C2H	C2H2	C2
C2H4	C2H4O2	C2H4O4	C2H5	C2H6	CH3N2CH3	C2H5OH	CH3OCH3	C2N	C2
C2O	C3	C3H60	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4N2	C5	C6H5	C6H5O	C6H6	C6H5OH	C7H8	C8
N-C8H18	I-C8H18	O-C12H9	C12H10	HCO	HCO	HCOO	H2O2	H2S	N
NO	NO2	NO2C2N2	NO2D	NO2D2H2	S	SH	SN	NaCN	NA
S2O	S8	V	VN	VO	VO2		SO	S2	

## SOLUTION 2

NaOH(A)	Na2O(C)	Na2O(A)	Na2O(L)	Na2SO4(IV)	Na2V2O6(S)	Na6V2O8(L)	V2O3(L)	V2O5(S)
<b>PURE SPECIES</b>								
C(G)	C7H8(L)	CBH18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	K2HBSO4(S)	NA(S)
NaOH(S)	NaOH(L)	NaO2(S)	Na2O3(I)	Na2O3(2)	Na2O3(L)	Na2O2(A)	Na2O2(B)	Na2S(L)
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	V0(S)
V02(S)	V02(S)	V02(L)						V0

CASE NO. B701 S21 0.1% SULFUR, 10 NA, 0.1 V PPM 182 iterations did not satisfy convergence requirements

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P, ATM 1.0000 1.0000 7.0000 7.0000  
 T, DEG K 1172.0 977.0 1172.0 977.0

## SOLUTION 1

AR 8.8009-3 8.8010-3 8.8009-3 8.8010-3  
 CO 3.0930-9 9.522-12 1.1690-9 3.599-12  
 CO2 9.0818-2 9.0818-2 9.0818-2 9.0819-2  
 H 5.870-12 4.831-15 1.384-12 1.123-15  
 HNO 1.515-12 1.651-14 2.464-12 2.686-14  
 HNO2 4.1223-9 1.6068-9 1.7740-9 6.9144-9  
 HNO3 1.207-11 1.511-11 1.374-10 1.720-10  
 H2 1.1960-8 9.707-10 1.9450-8 1.5790-9  
 H2 2.6110-9 1.616-11 9.868-10 6.106-12  
 H2O 9.6875-2 9.6877-2 9.6876-2 9.6877-2  
 H2O2 4.817-10 5.487-11 1.2740-9 1.452-10  
 H2SO4 2.711-10 8.1920-9 4.4500-9 9.2960-9  
 NO 9.4507-5 1.4826-5 9.4504-5 1.4826-5  
 NO2 1.0025-6 5.2001-7 2.4521-6 1.3757-6  
 N2 7.3702-1 7.3707-1 7.3702-1 7.3707-1  
 N2O 5.6021-9 1.0097-9 1.4821-8 2.6714-9  
 NA 4.546-12 1.474-17 9.864-14 3.843-19  
 NaOH 3.5140-8 4.614-12 3.2820-9 5.177-13  
 Na2SO4 6.5990-8 1.116-10 9.4440-9 1.594-11  
 O 3.4960-9 1.968-11 1.3210-9 7.437-12  
 OH 1.5470-6 5.5769-8 9.5107-7 3.4286-8  
 O2 6.6347-2 6.6382-2 6.6344-2 6.6377-2  
 O3 1.886-12 9.975-14 4.988-12 2.637-13  
 SO2 3.6511-5 2.4450-5 3.2361-5 1.4982-5  
 SO3 3.0702-6 1.5104-5 7.1996-6 2.4489-5  
 M, MOL WT 28.869 28.869 28.869 28.869  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0

## SOLUTION 2

NaOH(l) 2.9117-5 2.0239-7 1.9032-5 1.5896-7  
 Na2O(c) 1.745-12 0.000 0 0.000 0 0.000 0  
 Na2SiO3(s) 0.000 0 9.077-12 0.000 0 3.431-12  
 Na2SiO3(l) 3.5732-9 0.000000 1.3606-9 0.000000  
 Na2SO4(i) 0.000000 9.9549-1 0.000000 9.9549-1  
 Na2SO4(l) 9.9346-1 0.000000 9.9528-1 0.000000  
 Na2V2O6(l) 6.4598-3 4.3220-3 4.6882-3 2.9960-3  
 Na4V2O7(s) 4.7736-5 2.0107-8 2.1144-6 1.2293-9  
 Na6V2O8(s) 1.7180-9 0.000 0 4.644-12 0.000 0  
 V2O3(s) 3.646-12 2.857-12 6.195-12 3.214-12  
 V2O5(l) 1.1677-6 1.9201-4 1.3886-5 1.5104-3  
 M, MOL WT 142.70 142.48 142.51 142.40  
 PHASE FRACTION 1.8898-7 2.7249-7 2.6147-7 2.7295-7

## PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

## SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH2OH	CH3O	CH4	CH
CN	CH2	CNN	COS	CS	CS2	C2	C2H	C2	C2
C2H4	C2H402	C2H404	C2H5	C2H6	C2H5C2H3	C2H5OH	C2H5OCH3	C2H	C2
C2O	C3	C3H60	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
H-C4H10	I-C4H10	C4H2	C5	C4H5	C4H6	C4H5OH	C7H8	C8	C8
H-C8H18	I-C8H18	O-C12H24	C12H10	HCO	HCO	H2O2	H2S	N	N
NO	NH	NH2	NH3	N2S	N2H4	N2O4	N2O5	N3	NA
NAH	NaO	Na2	Na2C2H2	Na2O	Na2O2H2	S	SH	SN	SD
S2	S2O	S8	V	VN	VO	VO2			

## SOLUTION 2

NaOH(a)	Na2O(a)	Na2O(l)	Na2SO4(iv)	Na2V2O6(s)	Na6V2O8(l)	V2O3(l)	V2O3(s)					
PURE SPECIES												
C(gr)	C7H8(l)	C8H18(l)	H2O(s)	H2O(l)	H2SO4(l)	VN(s)	Na2HSO4(s)	NA(s)	NA			
NaCN(s)	NaCN(l)	NaO2(s)	Na2CO3(1)	Na2CO3(2)	Na2CO3(l)	Na2O2(A)	Na2O2(B)	Na2S(1)	NA			
Na2S(l)	S(s)	S(l)	V(s)	V(l)	NaV3O8(s)	Na2V12O31(s)	Na2V12O31(l)	VO(s)	VO			
VO2(s)	VO2(s)	VO2(l)										
M	2.000000	0	1.000000	0.000000	0.000000	0.000000	0.01000000	0.00	6	298.150	0	0.00000

CASE NO. 8701 122 0.1% SULFUR, 0.1 MA, 1.0 V PPM TIME = 0.609 SEC  
 P, ATM 1.0000 1.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

## SOLUTION 1

AR 8.8009-3 8.8009-3 8.8009-3 8.8010-3 8.8010-3 8.8010-3 8.8010-3 8.8010-3  
 CO 3.0930-9 9.522-12 1.1690-9 3.599-12 9.783-10 3.011-12 7.988-10 2.459-12  
 CO2 9.0818-2 9.0819-2 9.0819-2 9.0819-2 9.0819-2 9.0819-2 9.0819-2 9.0820-2  
 H 5.870-12 4.831-15 1.354-12 1.123-15 1.044-12 8.591-16 7.702-13 6.338-16  
 HNO 1.515-12 1.651-14 2.464-12 2.686-14 2.694-12 2.936-14 2.981-12 3.249-14  
 HNO2 4.1223-9 1.5068-9 1.7740-8 6.9143-9 2.3180-8 9.0349-9 3.1418-8 1.2246-8  
 HNO3 1.207-11 1.511-11 1.374-10 1.720-10 2.146-10 2.686-10 3.562-10 4.459-10  
 H2O 1.1960-9 9.707-10 1.9450-8 1.5790-9 2.1260-8 1.7260-9 2.3530-9 1.9100-9  
 H2 2.6110-9 1.616-11 9.868-10 6.106-12 8.256-10 5.109-12 6.741-10 4.172-12  
 H2O 9.6876-2 9.6877-2 9.6876-2 9.6878-2 9.6877-2 9.6878-2 9.6877-2 9.6878-2  
 H2O2 4.817-10 5.487-11 1.2740-9 1.452-10 1.5230-9 1.735-10 1.8450-9 2.125-10  
 H2SO4 2.729-10 8.2480-9 4.4810-9 9.3600-8 7.3880-9 1.4240-7 1.2960-8 2.2720-7  
 NO 9.4506-5 1.4826-5 9.4503-5 1.4825-5 9.4503-5 1.4825-5 9.4502-5 1.4825-5  
 NO2 1.0024-6 5.2000-7 2.6521-6 1.3757-6 3.1698-6 1.6442-6 3.8821-6 2.0137-6  
 NO3 1.257-13 2.790-14 8.801-13 1.946-13 1.257-12 2.779-13 1.886-12 4.169-13  
 N2 7.3702-1 7.3707-1 7.3702-1 7.3707-1 7.3702-1 7.3707-1 7.3702-1 7.3707-1  
 N2O 5.6021-9 1.0097-9 1.4821-8 2.6714-9 1.7715-8 3.1929-9 2.1496-8 3.9105-9  
 NaOH 2.446-10 5.007-13 9.383-11 1.455-13 7.850-11 1.098-13 6.400-11 7.789-14  
 Na2SO4 3.217-12 1.323-12 7.774-12 1.268-12 8.972-12 1.097-12 1.046-11 8.821-13  
 O 3.4960-9 1.968-11 1.3210-9 7.437-12 1.1060-9 6.222-12 9.027-10 5.080-12  
 OH 1.5470-6 5.5769-8 9.5107-7 3.4286-8 8.6794-7 3.1361-8 7.8807-7 2.8337-8  
 O2 6.6346-2 6.6381-2 6.6343-2 6.6376-2 6.6342-2 6.6375-2 6.6340-2 6.6374-2  
 O3 1.885-12 9.975-14 4.988-12 2.639-13 5.962-12 3.154-13 7.302-12 3.863-13  
 SO2 3.6745-5 2.4617-5 3.2582-5 1.5084-5 3.1462-5 1.3439-5 3.0040-5 1.1674-5  
 SO3 3.0899-6 1.5210-5 7.2497-6 2.4657-5 8.3659-6 2.6254-5 9.7828-6 2.7933-5  
 M, MOLE WT 28.869 28.869 28.869 28.869 28.869 28.869 28.869 28.869  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

## SOLUTION 2

NaOH(L) 2.0265-7 2.1963-8 5.4418-7 4.4681-8 6.5040-7 4.8144-8 7.9530-7 5.1248-8  
 Na2SO4(L) 0.000 0 0.000 0 1.120-12 0.000 0 1.545-12 0.000 0 2.205-12 0.000 0  
 Na2SO4(I) 0.000000 1.1804-2 0.000000 7.9189-2 0.000000 9.7896-2 0.000000 1.1802-1  
 Na2SO4(D) 4.8431-5 0.000000 8.1926-4 0.000000 1.3507-3 0.000000 2.3616-3 0.000000  
 Na2V2O6(L) 2.1132-1 2.0706-1 2.1614-1 1.2475-1 2.1602-1 1.0191-1 2.1525-1 7.7409-2  
 Na4V2O7(S) 7.5642-8 1.1344-8 7.9696-8 4.0408-9 7.9648-8 2.6829-9 7.9112-8 1.5394-9  
 V2O3(S) 2.4630-6 1.1630-8 3.4930-7 1.6940-9 2.4440-7 1.1920-9 1.6290-8 7.989-10  
 V2O5(L) 7.8863-1 7.8114-1 7.8304-1 7.9606-1 7.8263-1 8.0019-1 7.8238-1 8.0457-1  
 M, MOLE WT 194.98 194.24 195.24 186.46 195.21 184.30 195.13 181.98  
 PHASE FRACTION 1.2301-8 1.2447-8 1.2310-8 1.3358-8 1.2317-8 1.3635-8 1.2329-8 1.3946-8

## PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

## SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH20H	CH30	CH4	CH
CN	CH2	CNH	COS	CS	CS2	C2	C2H	C2	C2
C2H4	C2H4O2	C2H4O4	C2H5	C2H6	C2H3C2H3	C2H5OH	C2H3OCH3	C2N	C2
C2O	C3	C3H6O	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	CS	C4H5	C4H5O	C4H6	C4H5OH	C7H8	C8
N-C8H18	I-C8H18	O-C12H20	C12H10	HCO	HCO	HCO	H2O2	H2S	N
NCO	NH	NH2	NH3	NH4	N2O4	N2O5	N3	NA	NA
NAH	NAO	NA2	NA2C2H2	NA2O	NA2O2H2	S	SH	SN	SD
S2	S2O	S8	V	VN	VO	VO2			

## SOLUTION 2

NaOH(A)	Na2O(C)	Na2O(L)	Na2SO3(S)	Na2SO4(IV)	Na2V2O6(S)	Na4V2O8(S)	Na4V2O8(L)	V2
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## PURE SPECIES

C(Gr)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	N2H2SO4(S)	NA(S)	NA
NaOH(S)	NaOH(L)	NaO2(S)	Na2O3(S)	Na2O3(2)	Na2O3(L)	Na2O2(A)	Na2O2(B)	Na2S(1)	NA
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

CASE NO. 8701 222 0.1% SULFUR, 1.0 MA, 1.0 V PPM TIME = 0.749 SEC  
 P, ATM 1.0000 1.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0  
 SOLUTION 1  
 AR 8.8009-3 8.8009-3 8.8009-3 8.8010-3 8.8009-3 8.8010-3 8.8009-3 8.8010-3  
 CO 3.0930-9 9.522-12 1.1690-9 3.599-12 9.783-10 3.011-12 7.988-10 2.459-12  
 CO2 9.0818-2 9.0819-2 9.0819-2 9.0819-2 9.0819-2 9.0819-2 9.0819-2 9.0819-2  
 H 5.970-12 4.831-15 1.384-12 1.123-15 1.044-12 8.591-16 7.702-13 6.538-16  
 HNO 1.515-12 1.651-14 2.464-12 2.686-14 2.694-12 2.936-14 2.981-12 3.249-14  
 HNO2 4.1223-9 1.6068-9 1.7740-8 6.9144-9 2.3180-8 9.0349-9 3.1418-8 1.2246-8  
 HNO3 1.207-11 1.511-11 1.374-10 1.720-10 2.146-10 2.686-10 3.562-10 4.459-10  
 H2 1.1960-8 9.707-10 1.9450-8 1.5790-9 2.1260-8 1.7260-9 2.3530-8 1.9100-9  
 H2 2.6110-9 1.616-11 9.868-10 6.106-12 8.256-10 5.109-12 6.741-10 4.172-12  
 H2O 9.6876-2 9.6877-2 9.6878-2 9.6879-2 9.6876-2 9.6877-2 9.6878-2 9.6879-2  
 H2O2 4.817-10 5.487-11 1.2740-9 1.452-10 1.5230-9 1.735-10 1.8650-9 2.125-10  
 H2SO4 2.728-10 8.2450-9 4.4790-9 9.3550-8 7.3850-9 1.4230-7 1.2750-8 2.2710-7  
 NO 9.4506-5 1.4826-5 9.4504-5 1.4825-5 9.4503-5 1.4825-5 9.4502-5 1.4825-5  
 NO2 1.0024-6 5.2000-7 2.6521-6 1.3737-6 3.1698-6 1.6442-6 3.8821-6 2.0137-6  
 NO3 1.257-13 2.780-14 8.801-13 1.946-13 1.257-12 2.779-13 1.086-12 4.169-13  
 N2 7.3702-1 7.3702-1 7.3702-1 7.3702-1 7.3702-1 7.3702-1 7.3702-1 7.3702-1  
 N2O 5.6021-9 1.0097-9 1.4821-8 2.6714-9 1.7715-8 3.1929-9 2.1696-8 3.9105-9  
 NA 1.527-12 1.104-17 6.554-14 3.033-19 3.391-14 1.592-19 1.586-14 7.671-20  
 NaOH 1.1810-8 3.456-12 2.1800-9 4.087-13 1.4740-9 2.803-13 9.344-10 1.630-13  
 Na2SO4 7.4950-9 6.302-11 4.1960-9 9.999-12 3.1630-9 7.151-12 2.2290-9 4.868-12  
 O 3.4960-9 1.968-11 1.3210-9 7.437-12 1.1060-9 6.222-12 9.027-10 5.080-12  
 OH 1.5470-6 5.5769-8 9.5107-7 3.4284-6 8.6994-7 3.1361-8 7.8607-7 2.8337-8  
 O2 6.6346-2 6.6381-2 6.6343-2 6.6376-2 6.6342-2 6.6375-2 6.6340-2 6.6374-2  
 O3 1.885-12 9.975-14 4.988-12 2.639-13 5.962-12 3.154-13 7.302-12 3.863-13  
 SO2 3.6737-5 2.4608-5 3.2571-5 1.5077-5 3.1451-5 1.3431-5 3.0029-5 1.1668-5  
 SO3 3.0892-6 1.5204-5 7.2462-6 2.4645-5 8.3629-6 2.6241-5 9.7792-6 2.7918-5  
 M, MOLE WT 28.869 28.869 28.869 28.869 28.869 28.869 28.869 28.869  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0  
 SOLUTION 2  
 NaOH(L) 9.7828-6 1.5160-7 1.2644-5 1.2549-7 1.2213-5 1.2293-7 1.1612-5 1.2043-7  
 Na2SO3(S) 0.000 0 5.126-12 0.000 0 2.152-12 0.000 0 1.839-12 0.000 0 1.534-12  
 Na2SO3(L) 4.081-10 0.000 0 6.044-10 0.000 0 5.446-10 0.000 0 4.700-10 0.000 0  
 Na2SO4(I) 0.000000 5.6216-1 0.000000 6.2437-1 0.000000 6.3789-1 0.000000 6.5138-1  
 Na2SO4(L) 1.1284-1 0.000000 4.4214-1 0.000000 4.7611-1 0.000000 5.0330-1 0.000000  
 Na2V2O6(L) 8.8500-1 4.0571-1 5.5402-1 2.0765-1 5.1848-1 1.6427-1 4.8832-1 1.2096-1  
 Na4V2O7(S) 7.3824-4 1.0591-6 1.1029-4 5.3058-8 6.7410-5 2.8192-8 3.8263-5 1.3282-8  
 Na6V2O8(S) 2.9990-9 0.000 0 1.069-10 0.000 0 4.269-11 0.000 0 1.460-11 0.000 0  
 V2O3(S) 4.4230-9 4.784-10 1.6590-9 3.574-10 1.6640-9 2.947-10 1.7330-9 2.261-10  
 V2O5(L) 1.4172-3 3.2125-2 3.7178-3 1.6797-1 5.3272-3 1.9784-1 8.3250-3 2.2766-1  
 M, MOLE WT 232.33 184.63 198.61 169.87 195.05 166.65 192.10 163.42  
 PHASE FRACTION 1.3865-8 2.8093-8 2.2050-8 3.2746-8 2.3479-8 3.3969-8 2.4765-8 3.5284-8  
 PURE SPECIES PHASE FRACTIONS (IF ANY)  
 ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS  
 SOLUTION 1  

C	CH	CH2	CH2D	CH2D2	CH3	CH2OH	CH3O	CH4	CH
CN	CN2	CN4	COS	CS	CS2	C2	C2H	C2R2	C2
C2H4	C2H4O2	C2H4O4	C2H5	C2H6	C2H2C2H3	C2H5OH	C2H3OCH3	C2N	C2
C2O	C3	C3H6O	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	C5	C6H5	C6H5O	C6H6	C6HSOH	C7H8	C8
N-C8H18	I-C8H18	O-C12H9	C12H10	HCO	HCO	HCO	H2N2	H2S	N
NO	NH	NH2	NH3	N2H4	N2O4	N2O5	N3	NACH	NA
NaO	Na2	Na2C2H2	Na2O	Na2O2H2	S	SH	SN	SD	S2
SO2	S8	V	VN	VO	V2				

 SOLUTION 2

NaOH(A)	Na2O(C)	Na2O(A)	Na2O(L)	Na2SO4(IV)	Na2V2O6(S)	Na6V2O8(L)	V2O3(L)	V2O5(S)
<b>PURE SPECIES</b>								
C(6R)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	Na2HSO4(S)	Na(S)
NaCN(S)	NaCN(L)	Na2O2(S)	Na2CO3(1)	Na2CO3(2)	Na2CO3(L)	Na2O2(A)	Na2O2(B)	Na2S(1)
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	VO(S)
VO2(S)	VO2(L)							VO

CASE NO. 8701 322 0.1% SULFUR, 10 NA, 1.0 V PPM singular matrix, iteration 30 variable 7

P, ATM 1.0000 1.0000  
T, DEG K 1172.0 977.0

## SOLUTION 1

AR 8.8009-3 8.8010-3  
CO 3.0930-9 9.522-12  
CO2 9.0817-2 9.0818-2  
H 5.870-12 4.831-15  
HNO 1.515-12 1.651-14  
HNO2 4.1223-9 1.6068-9  
HNO3 1.207-11 1.511-11  
HO2 1.1960-8 9.707-10  
H2 2.6110-9 1.616-11  
H2O 9.6875-2 9.6876-2  
H2O2 4.817-10 5.487-11  
H2SO4 2.712-10 8.1940-9  
NO 9.4507-5 1.4826-5  
NO2 1.0025-6 5.2001-7  
N2 7.3702-1 7.3707-1  
N2O 5.6021-9 1.0097-9  
NA 4.413-12 1.443-17  
NAOH 3.4110-8 4.519-12  
Na2SO4 6.2190-8 1.071-10  
O 3.4960-9 1.968-11  
OH 1.5470-6 5.5769-8  
O2 6.6347-2 6.6382-2  
O3 1.886-12 9.975-14  
SO2 3.6521-5 2.4456-5  
SO3 3.0710-6 1.5110-5  
M, MOL WT 28.889 28.889  
PHASE FRACTION 1.0000 0 1.0000 0

## SOLUTION 2

NaOH(L) 2.8263-5 1.9820-7  
Na2O(C) 1.644-12 0.000 0  
Na2SO3(S) 0.000 0 8.707-12  
Na2SO3(L) 3.3865-9 0.000000  
Na2SO4(I) 0.000000 9.5494-1  
Na2SO4(L) 9.3631-1 0.000000  
Na2V2O6(L) 6.3207-2 4.3063-2  
Na4V2O7(S) 4.4009-4 1.9213-7  
Na6V2O8(S) 1.4925-8 0.000000  
V2O3(S) 3.787-11 2.971-11  
V2O5(L) 1.2127-5 1.9949-3  
M, MOL WT 148.54 146.50  
PHASE FRACTION 1.9322-7 2.7299-7

## PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

## SOLUTION 1

C	CH	CH2	CH2O	CH2O2	CH3	CH2OH	CH3O	CH4	CH
CN	CH2	CNN	COS	CS	CS2	C2	C2H	C2H2	C2
C2H4	C2H4O2	C2H4O4	C2H5	C2H6	CH3K2CH3	C2H5OH	CH3OCH3	C2N	C2
C2O	C3	C3H6O	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	CS	C4H5	C4H5O	C4H6	C4H5OH	C7H8	C8
N-C8H18	I-C8H18	O-C12H29	C12H10	HCO	HCO	HCO	H2O2	H2S	N
NO	NH	NH2	NH3	NH3	NH4	NH4	N2O4	N2O5	NA
NAH	NAO	NA2	NA2C2N2	NA2O	NA2O2H2	S	SH	SN	SO
S2	S2O	S8	V	VN	VO	VO2			

## SOLUTION 2

NaOH(A)	Na2O(A)	Na2O(L)	Na2SO4(IV)	Na2V2O6(S)	Na6V2O8(L)	V2O3(L)	V2O5(S)	
PURE SPECIES								
C(GR)	C7H8(L)	CBH18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	Na2HSO4(S)	NA(S)
NaOH(S)	NaOH(L)	NaO2(S)	Na2O3(I)	Na2O3(2)	Na2O3(L)	Na2O2(A)	Na2O2(B)	Na2S(I)
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	VO(S)
VO2(S)	VO2(S)	VO2(L)						VO

CASE NO. 8701 123 0.1% SULFUR, 0.1 NA, 10 V PPM TIME = 0.598 SEC  
 P, ATM 1.0000 1.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

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SOLUTION 1

AR 8.8009-3 8.8010-3 8.8009-3 8.8010-3 8.8009-3 8.8010-3 8.8009-3 8.8010-3  
 CO 3.0930-9 9.522-12 1.1690-9 3.599-12 9.783-10 3.011-12 7.988-10 2.459-12  
 CO2 9.0818-2 9.0818-2 9.0818-2 9.0818-2 9.0818-2 9.0818-2 9.0818-2 9.0818-2  
 H 5.870-12 4.831-15 1.384-12 1.123-15 1.044-12 8.591-16 7.702-13 6.338-16  
 HNO 1.515-12 1.651-14 2.464-12 2.686-14 2.694-12 2.936-14 2.981-12 3.249-14  
 HNO2 4.1223-9 1.5068-9 1.7740-8 6.9144-9 2.3181-8 9.0350-9 3.1419-8 1.2246-8  
 HNO3 1.207-11 1.511-11 1.374-10 1.720-10 2.146-10 2.686-10 3.562-10 4.459-10  
 HO2 1.1960-8 9.707-10 1.9450-8 1.5790-9 2.1260-8 1.7260-9 2.3530-8 1.9100-9  
 H2 2.6110-9 1.616-11 9.868-10 6.106-12 8.256-10 5.109-12 6.741-10 4.171-12  
 H2O 9.6875-2 9.6876-2 9.6876-2 9.6877-2 9.6877-2 9.6877-2 9.6877-2 9.6877-2  
 H2O2 4.817-10 5.487-11 1.2740-9 1.452-10 1.5230-9 1.735-10 1.8850-9 2.125-10  
 H2SO4 2.729-10 8.2480-9 4.4810-9 9.3800-8 7.3880-9 1.4240-7 1.2960-8 2.2720-7  
 NO 9.4507-5 1.4826-5 9.4504-5 1.4826-5 9.4503-5 1.4825-5 9.4503-5 1.4825-5  
 NO2 1.0025-6 5.2001-7 2.6521-6 1.3757-6 3.1698-6 1.6443-6 3.8822-6 2.0138-6  
 NO3 1.257-13 2.780-14 8.801-13 1.946-13 1.257-12 2.779-13 1.886-12 4.169-13  
 N2 7.3702-1 7.3707-1 7.3702-1 7.3707-1 7.3702-1 7.3707-1 7.3702-1 7.3707-1  
 N2O 5.6021-9 1.0097-9 1.4821-8 2.6714-9 1.7715-8 3.1930-9 2.1696-8 3.9105-9  
 NaOH 7.065-11 1.431-13 2.678-11 4.476-14 2.239-11 3.447-14 1.825-11 2.502-14  
 O 3.4960-9 1.968-11 1.3210-9 7.437-12 1.1060-9 6.222-12 9.027-10 5.080-12  
 OH 1.5470-6 5.5769-8 9.5107-7 3.4284-8 8.6994-7 3.1361-8 7.8807-7 2.8337-8  
 O2 6.6347-2 6.6382-2 6.6344-2 6.6377-2 6.6343-2 6.6376-2 6.6341-2 6.6375-2  
 O3 1.886-12 9.975-14 4.988-12 2.639-13 5.962-12 3.154-13 7.302-12 3.863-13  
 SO2 3.6745-5 2.4617-5 3.2582-5 1.5084-5 3.1462-5 1.3438-5 3.0040-5 1.1674-5  
 SO3 3.0899-6 1.5210-5 7.2487-6 2.4657-5 8.3659-6 2.6254-5 9.7828-6 2.7933-5  
 M, MOLE WT 28.869 28.869 28.869 28.869 28.869 28.869 28.869 28.869  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

SOLUTION 2

NaOH(L) 5.8534-8 6.2772-9 1.5529-7 1.3743-8 1.8549-7 1.5121-8 2.2683-7 1.6462-8  
 Na2SO4(I) 0.000000 9.6415-4 0.000000 7.4920-3 0.000000 9.6567-3 0.000000 1.2178-2  
 Na2SO4(L) 4.0406-6 0.000000 6.6713-5 0.000000 1.0986-4 0.000000 1.9212-4 0.000000  
 Na2V2O6(L) 2.1867-2 2.1173-2 2.1981-2 1.4500-2 2.1953-2 1.2288-2 2.1888-2 9.7104-3  
 Na4V207(S) 6.530-10 9.475-11 6.600-10 4.444-11 6.584-10 3.191-11 6.544-10 1.972-11  
 V2O3(S) 3.0540-6 1.4560-8 4.3630-7 2.0810-9 3.0540-7 1.4570-9 2.0360-7 9.712-10  
 V2O5(L) 9.7813-1 9.7786-1 9.7795-1 9.7801-1 9.7794-1 9.7806-1 9.7792-1 9.7811-1  
 M, MOLE WT 183.24 183.15 183.24 182.48 183.24 182.26 183.23 182.00  
 PHASE FRACTION 1.2300-7 1.2312-7 1.2301-7 1.2393-7 1.2302-7 1.2420-7 1.2303-7 1.2452-7

PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH20H	CH30	CH4	CH
CN	CN2	CN3	COS	C3	C5	C2	C2H	C2	C2
C2H4	C2H402	C2H404	C2H5	C2H6	C3H2CH3	C2H50H	C3H3CH3	C2N	C2
C20	C3	C3H60	M-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
M-C4H10	I-C4H10	C4H2	C5	C6H5	C6H50	C6H6	C6H5OH	C7H8	C8
M-C8H18	I-C8H18	O-C12H9	C12H10	HCO	HCO	HCO	H2N2	H2S	N
NO	NH	NH2	NH3	N2H4	N2O4	N2S	NO	NA	NA
NAH	NAO	NA2	NA2C2H2	NA20	NA20H2	NA2S04	S	SH	SN
SO	S2	S20	S8	V	VN	VO	VO2		

SOLUTION 2

NaOH(A)	Na2O(C)	Na2O(A)	Na2O(L)	Na2S03(S)	Na2S03(L)	Na2S04(IV)	Na2V2O6(S)	Na4V2O8(S)	NA
V2O3(L)	V2O5(S)								

PURE SPECIES

C(GR)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2S04(L)	VN(S)	N2H5S04(S)	NA(S)	NA
NaOH(S)	NaOH(L)	NaO2(S)	Na2O3(S)	Na2O3(2)	Na2O3(L)	Na2O2(A)	Na2O2(B)	Na2S(1)	NA

Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

CASE NO. 8701 223 0.1% SULFUR, 1.0 NA, 10 V PPM TIME = 0.603 SEC  
 P, ATM 1.0000 1.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

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SOLUTION 1

AR 8.8009-3 8.8010-3 8.8009-3 8.8010-3 8.8009-3 8.8010-3 8.8009-3 8.8010-3  
 CO 3.0930-9 9.522-12 1.1690-9 3.599-12 9.783-10 3.011-12 7.988-10 2.459-12  
 CO2 9.0817-2 9.0818-2 9.0818-2 9.0819-2 9.0818-2 9.0819-2 9.0818-2 9.0819-2  
 H 5.870-12 4.831-15 1.364-12 1.123-15 1.044-12 8.591-16 7.702-13 6.338-16  
 HNO 1.515-12 1.651-14 2.464-12 2.686-14 2.694-12 2.936-14 2.981-12 3.249-14  
 HNO2 4.1223-9 1.6068-9 1.7740-8 6.9144-9 2.3181-8 9.0350-9 3.1419-8 1.2246-8  
 HNO3 1.207-11 1.511-11 1.374-10 1.720-10 2.146-10 2.684-10 3.542-10 4.459-10  
 H2O 1.1960-8 9.707-10 1.9450-8 1.5790-9 2.1260-8 1.7260-9 2.3530-8 1.9100-9  
 H2 2.6110-9 1.616-11 9.868-10 6.106-12 8.256-10 5.109-12 6.741-10 4.171-12  
 H2O 9.6875-2 9.6876-2 9.6876-2 9.6877-2 9.6876-2 9.6877-2 9.6876-2 9.6877-2  
 H2O2 4.817-10 5.487-11 1.2740-9 1.452-10 1.5230-9 1.735-10 1.8650-9 2.125-10  
 H2SO4 2.729-10 8.2480-9 4.4810-9 9.3580-8 7.3880-9 1.4230-7 1.2960-8 2.2710-7  
 NO 9.4507-5 1.4825-5 9.4504-5 1.4825-5 9.4504-5 1.4825-5 9.4503-5 1.4825-5  
 NO2 1.0025-6 5.2001-7 2.6521-6 1.3757-6 3.1698-6 1.6443-6 3.8822-6 2.0139-6  
 NO3 1.257-13 2.780-14 8.801-13 1.946-13 1.257-12 2.779-13 1.886-12 4.169-13  
 N2 7.3702-1 7.3707-1 7.3702-1 7.3707-1 7.3702-1 7.3707-1 7.3702-1 7.3707-1  
 N2O 5.6021-9 1.0097-9 1.4821-8 2.6714-9 1.7715-8 3.1930-9 2.1696-8 3.9105-9  
 NaOH 2.513-10 5.009-13 9.493-11 1.456-13 7.931-11 1.098-13 6.457-11 7.790-14  
 Na2SO4 3.396-12 1.324-12 7.957-12 1.269-12 9.158-12 1.098-12 1.045-11 8.820-13  
 O 3.4960-9 1.968-11 1.3210-9 7.437-12 1.1060-9 6.222-12 9.027-10 5.080-12  
 OH 1.5470-6 5.5769-8 9.5107-7 3.4286-8 8.6994-7 3.1361-8 7.8607-7 2.8337-8  
 O2 6.6347-2 6.6382-2 6.6344-2 6.6377-2 6.6343-2 6.6376-2 6.6341-2 6.6375-2  
 O3 1.886-12 9.975-14 4.988-12 2.639-13 5.962-12 3.154-13 7.302-12 3.863-13  
 SO2 3.6745-5 2.4616-5 3.2582-5 1.5080-5 3.1462-5 1.3434-5 3.0039-5 1.1669-5  
 SO3 3.0899-6 1.5209-5 7.2487-6 2.4651-5 8.3659-6 2.6246-5 9.7827-6 2.7923-5  
 M, MOLE WT 28.849 28.849 28.849 28.849 28.849 28.849 28.849 28.849  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

SOLUTION 2

NaOH(L) 2.0820-7 2.1969-8 5.5035-7 4.4673-8 6.5710-7 4.8157-8 8.0246-7 5.1225-8  
 Na2SO4(L) 0.000 0 0.000 0 1.146-12 0.000 0 1.577-12 0.000 0 2.245-12 0.000 0  
 Na2SO4(I) 0.000000 1.1810-2 0.000000 7.9213-2 0.000000 9.7918-2 0.000000 1.1801-1  
 Na2SO4(L) 5.1122-5 0.000000 8.3857-4 0.000000 1.3787-3 0.000000 2.4044-3 0.000000  
 Na2V2O6(L) 2.2047-1 2.0715-1 2.2011-1 1.2481-1 2.1950-1 1.0196-1 2.1830-1 7.7428-2  
 Na4V2O7(S) 8.3303-8 1.1335-8 8.3073-8 4.0449-9 8.2609-8 2.6855-9 8.1686-8 1.5401-9  
 V2O3(S) 2.4340-6 1.1630-8 3.4750-7 1.6940-9 2.4330-7 1.1920-9 1.6220-7 7.989-10  
 V2O5(L) 7.7947-1 7.8104-1 7.7905-1 7.9598-1 7.7912-1 8.0012-1 7.7930-1 8.0457-1  
 M, MOLE WT 195.54 194.25 195.49 186.46 195.43 184.30 195.31 181.98  
 PHASE FRACTION 1.2301-7 1.2447-7 1.2311-7 1.3358-7 1.2317-7 1.3635-7 1.2330-7 1.3946-7

PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH20H	CH50	CH4	CH
CH	CH2	CHM	CH6	CS	CS2	C2	C2H	C2H2	C2
C2H4	C2H402	C2H404	C2H5	C2H6	CH3CH2CH3	C2H60H	CH3COCH3	C2N	C2
C20	C3	C3H60	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	C5	C4H5	C4H50	C4H6	C4H50H	C7H8	C8
N-C8H18	I-C8H18	O-C12H9	C12H10	HCO	HCO	HCO	H2O2	H2S	N
NO	NH	NH2	NH3	NH4	N2O4	N2O5	N3	NA	NA
NA	NAO	NA2	NA2C2H2	NA20	NA2O2H2	S	SH	SN	SO
S2	S2O	S8	V	VN	VO	VO2			

SOLUTION 2

NaOH(A)	Na2O(C)	Na2O(L)	Na2SO3(S)	Na2SO4(IV)	Na2V2O6(S)	Na4V2O8(S)	Na4V2O8(L)	V2
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PURE SPECIES

C(6R)	C7H8(L)	CH3H18(L)	H2O(S)	H2O(L)	Na2SO4(L)	VN(S)	Na2HSO4(S)	NA(S)	NA
NaOH(S)	NaOH(L)	NaO2(S)	Na2O3(I)	Na2O3(2)	Na2O3(L)	Na2O2(A)	Na2O2(B)	Na2S(1)	NA
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

CASE NO. 8701 323 0.1% SULFUR, 10 NA, 10 V PPM Osingular matrix, iteration 30 variable 1

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P, ATM 1.0000 1.0000

T, DEG K 1172.0 977.0

## SOLUTION 1

AR 8.8009-3 8.8010-3

CO 3.0930-9 9.521-12

CO2 9.0817-2 9.0817-2

H 5.870-12 4.831-15

HNO 1.515-12 1.651-14

HNO2 4.1224-9 1.6068-9

HNO3 1.207-11 1.511-11

HO 1.1960-8 9.708-10

H2 2.6110-9 1.615-11

H2O 9.6874-2 9.6876-2

H2O2 4.817-10 5.487-11

H2SO4 2.719-10 8.2150-9

NO 9.4507-5 1.4826-5

NO2 1.0025-6 5.2002-7

N2 7.3702-1 7.3707-1

N2O 5.6022-9 1.0098-9

NA 3.102-12 1.107-17

NAOH 2.3980-8 3.465-12

NA2SO4 3.0800-8 6.312-11

O 3.4960-9 1.968-11

OH 1.5470-6 5.5769-8

O2 6.6348-2 6.6383-2

O3 1.886-12 9.975-14

SO2 3.6618-5 2.4519-5

SO3 3.0792-6 1.5149-5

M, MOLE WT 28.869 28.869

PHASE FRACTION 1.0000 0 1.0000 0

## SOLUTION 2

NAOH(L) 1.9865-5 1.5199-7

NA2SO3(S) 0.000 0 5.133-12

NA2SO3(L) 1.6773-9 0.000000

NA2SO4(I) 0.000000 5.6300-1

NA2SO4(L) 4.6376-1 0.000000

NA2V2O6(L) 5.3418-1 4.0509-1

NA4V2O7(S) 1.8373-3 1.0628-6

NA6V2O8(S) 3.0778-8 0.000000

V2O3(S) 6.478-10 4.752-10

V2O5(L) 2.0747-4 3.1912-2

M, MOLE WT 196.74 184.56

PHASE FRACTION 2.2938-7 2.8147-7

## PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

## SOLUTION 1

C	CH	CH2	CH2O	CH2O2	CH3	CH2OH	CH3O	CH4	CH
CN	CH2	CH3	CH3	CS	CS2	C2	C2H	C2H2	C2
C2H4	C2H4O2	C2H4O4	C2H5	C2H6	C3H2CH3	C2H5OH	C3H3OCH3	C2N	C2
C2O	C3	C3H6O	H-C3H7	I-C3H7	C3H8	1-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	C5	C6H5	C6H5O	C6H6	C6H5OH	C7H8	C8
N-C8H18	I-C8H18	O-C12H9	C12H10	HON	HOD	HNCO	H2N2	H2S	N
NO	NH	NH2	NH3	NH3	N2H4	N2O4	N2O5	N3	NA
NH	NAO	NA2	NA2C2H2	NA2O	NA2O2H2	S	SH	SN	SO
S2	S2O	S8	V	VN	VO	VO2			

## SOLUTION 2

NAOH(A) NA2O(C) NA2O(A) NA2O(L) NA2SO4(IV) NA2V2O6(S) NA6V2O8(L) V2O3(L) V2O5(S)

## PURE SPECIES

C(Gr)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	N2HBSO4(S)	NA(S)	NA
NA(O(S))	NA(O(L))	NA(O(S))	NA2CO3(1)	NA2CO3(2)	NA2CO3(L)	NA2O2(A)	NA2O2(B)	NA2S(L)	NA
NA2S(L)	S(S)	S(L)	V(S)	V(L)	NAV3O8(S)	NA2V12O31(S)	NA2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

STOP

## SOLN 1 GASES

SOLN 2 V205(L) V203(L) V204(L)  
 SOLN 2 Na2S03(L) Na2S04(L) NaOH(L)  
 SOLN 2 Na2O(L) Na2V206(S) Na4V207(S) Na6V208(S)

CASE NO. 8701 131 1.0% SULFUR, 0.1 NA, 0.1 V PPM  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

## SOLUTION 1

AR 8.8043-3 8.8048-3 8.8044-3 8.8052-3 8.8045-3 8.8052-3 8.8053-3  
 CO 3.0470-9 9.383-12 1.3630-9 4.199-12 1.1520-9 3.548-12 9.639-10 2.969-12  
 CO2 9.0030-2 9.0036-2 9.0032-2 9.0039-2 9.0032-2 9.0040-2 9.0033-2 9.0041-2  
 H 5.830-12 4.799-15 1.744-12 1.435-15 1.355-12 1.115-15 1.037-12 8.534-16  
 HNO 1.514-12 1.651-14 2.265-12 2.468-14 2.463-12 2.684-14 2.693-12 2.735-14  
 HNO2 4.1475-9 1.6158-9 1.3866-8 5.4006-9 1.7845-8 6.9503-9 2.3317-8 9.0812-9  
 HNO3 1.222-11 1.528-11 9.133-11 1.142-10 1.391-10 1.739-10 2.172-10 2.715-10  
 HO2 1.2030-8 9.760-10 1.7980-8 1.4590-9 1.9560-8 1.5870-9 2.1380-8 1.7350-9  
 H2 2.5750-9 1.594-11 1.1520-9 7.132-12 9.736-10 6.029-12 8.146-10 5.044-12  
 H2O 9.6172-2 9.6178-2 9.6174-2 9.6182-2 9.6174-2 9.6182-2 9.6175-2 9.6182-2  
 H2O2 4.812-10 5.480-11 1.0760-9 1.225-10 1.2730-9 1.449-10 1.5220-9 1.732-10  
 H2S04 2.7009-9 8.1478-8 2.7537-8 6.1724-7 4.4321-8 9.2328-7 7.3061-8 1.4041-6  
 NO 9.5128-5 1.4918-5 9.5117-5 1.4914-5 9.5114-5 1.4914-5 9.5110-5 1.4913-5  
 NO2 1.0155-6 5.2638-7 2.2702-6 1.1764-6 2.6859-6 1.3918-6 3.2100-6 1.6633-6  
 NO3 1.282-13 2.831-14 6.407-13 1.414-13 8.969-13 1.980-13 1.281-12 2.827-13  
 N2 7.3731-1 7.3739-1 7.3732-1 7.3742-1 7.3732-1 7.3743-1 7.3732-1 7.3743-1  
 N2O 5.6400-9 1.0162-9 1.2610-8 2.2719-9 1.4920-8 2.6880-9 1.7832-8 3.2126-9  
 NaOH 1.3280-9 1.139-12 6.598-10 2.509-12 3.859-10 1.344-13 3.987-10 1.663-12  
 Na2S04 9.519-10 6.864-11 2.3970-9 2.5220-9 1.3200-9 1.083-11 2.3220-9 2.5210-9  
 O 3.5190-9 1.979-11 1.5730-9 8.850-12 1.3300-9 7.479-12 1.1120-9 6.257-12  
 OH 1.5463-6 5.5734-8 1.0340-6 3.7267-8 9.5058-7 3.4260-8 8.6947-7 3.1334-8  
 O2 6.7196-2 6.7181-2 6.7180-2 6.7144-2 6.7176-2 6.7134-2 6.7170-2 6.7128-2  
 O3 1.922-12 1.016-13 4.296-12 2.269-13 5.082-12 2.684-13 6.074-12 3.208-13  
 SO2 3.6407-4 2.4349-4 3.3204-4 1.6502-4 3.2262-4 1.4902-4 3.1148-4 1.3273-4  
 SO3 3.0810-5 1.5134-4 6.2824-5 2.2929-4 7.2224-5 2.4498-4 8.3340-5 2.6079-4  
 M, MOLE WT 28.880 28.882 28.880 28.883 28.880 28.883 28.881 28.883  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

## SOLUTION 2

NaOH(L) 1.0999-6 4.9968-8 0.000000 0.000000 2.2383-6 4.1273-8 0.000000 0.000000  
 Na2S03(S) 0.000 0 5.550-12 0.000 0 0.000 0 0.000 0 2.317-12 0.000 0 0.000 0  
 Na2S03(L) 5.150-11 0.000 0 0.000 0 0.000 0 1.890-10 0.000 0 0.000 0 0.000 0  
 Na2S04(I) 0.000000 6.1231-1 0.000000 0.000000 0.000000 6.7620-1 0.000000 0.000000  
 Na2S04(L) 1.4330-2 0.000000 0.000000 0.000000 1.3711-1 0.000000 0.000000 0.000000  
 Na2V206(L) 8.7555-1 2.2493-1 0.000000 0.000000 7.0796-1 3.8434-2 0.000000 0.000000  
 Na4V207(S) 9.2998-6 6.4247-8 0.000000 0.000000 0.000000 1.0699-9 0.000000 0.000000  
 V203(S) 3.3950-7 2.3950-9 0.000 0 0.000 0 6.6500-8 6.003-10 0.000 0 0.000 0  
 V205(L) 1.1011-1 1.6276-1 0.000000 0.000000 1.5093-1 2.8536-1 0.000000 0.000000  
 M, MOLE WT 235.58 171.42 0.0000 0.0000 220.34 157.32 0.0000 0.0000  
 PHASE FRACTION 1.2484-9 3.1742-9 0.000000 0.000000 1.4294-9 3.8006-9 0.000000 0.000000  
 PURE SPECIES PHASE FRACTIONS (IF ANY)

Na2V12031(L) 0.000 0 0.000 0 0.000 0 2.051-10 0.000 0 0.000 0 2.051-10 2.051-10

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

## SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH20H	CH30	CH4	CH
CN	CN2	CN	COS	CS	CS2	C2	C2H	C2H2	C2
C2H4	C2H402	C2H404	C2H5	C2H6	C2H5C2H3	C2H5OH	C2H3C2H3	C2N	C2

C20	C3	C3H60	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	C5	C4H5	C4H50	C4H6	C4H5OH	C7H8	C8
N-C8H18	I-C8H18	0-C12H9	C12H10	HON	HCO	HNO2	H2N2	H2S	N
NCO	NH	NH2	NH3	N2H4	N2O4	N2O5	N3	NA	NA
NAH	NAO	NA2	NA2C2N2	NA20	NA2O2H2	S	SH	SN	SO
S2	S20	S8	V	VN	VO	VO2			
SOLUTION 2									
NaOH(A)	Na2O(C)	Na2O(A)	Na2O(L)	Na2S04(IV)	Na2V206(S)	Na6V208(S)	Na6V208(L)	V203(L)	V2
PURE SPECIES									
C(GR)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2S04(L)	VN(S)	N2H8S04(S)	NA(S)	NA
NaCN(S)	NaCN(L)	Na2O2(S)	Na2C03(1)	Na2C03(2)	Na2C03(L)	Na2O2(A)	Na2O2(B)	Na2S(1)	NA
Na2S(L)	S(S)	S(L)	V(S)	V(L)	Na3S08(S)	Na2V12031(S)	VO(S)	VO(L)	VO
VO2(S)	VO2(L)								

CASE NO.	8701	231	1.0% SULFUR,	1.0 NA,	0.1 V PPM	TIME =	0.559 SEC
P, ATM		1.0000	1.0000	5.0000	5.0000	7.0000	10.000
T, DEG K		1172.0	977.0	1172.0	977.0	1172.0	977.0
SOLUTION 1							
AR		8.8043-3	8.8048-3	8.8044-3	8.8052-3	8.8045-3	8.8053-3
CO		3.0470-9	9.383-12	1.3830-9	4.198-12	1.1520-9	3.548-12
CO2		9.0030-2	9.0035-2	9.0032-2	9.0039-2	9.0040-2	9.0033-2
H		5.830-12	4.799-15	1.744-12	1.435-15	1.355-12	1.115-15
HNO		1.514-12	1.651-14	2.245-12	2.468-14	2.463-12	2.684-14
HNO2		4.1475-9	1.6158-9	1.3866-8	5.4006-8	1.7845-9	6.9503-9
HNO3		1.222-11	1.528-11	9.133-11	1.142-10	1.391-10	1.739-10
H2O		1.2030-8	9.760-10	1.7980-8	1.4590-9	1.9560-8	1.5870-9
H2		2.5750-9	1.594-11	1.1520-9	7.132-12	9.736-10	6.028-12
H2O2		9.6172-2	9.6178-2	9.6173-2	9.6181-2	9.6174-2	9.6182-2
H2SO4		4.812-10	5.480-11	1.0760-9	1.225-10	1.2730-9	1.449-10
N		2.7008-9	8.1473-8	2.7536-8	6.1720-7	4.4318-8	9.2323-7
NO		9.5129-5	1.4918-5	9.5117-5	1.4914-5	9.5114-5	1.4914-5
NO2		1.0155-6	5.2638-7	2.2702-7	1.1764-6	2.6859-6	1.3918-6
NO3		1.282-13	2.831-14	6.407-13	1.414-13	8.969-13	1.980-13
N2		7.3731-1	7.3739-1	7.3732-1	7.3742-1	7.3743-1	7.3742-1
N2O		5.6400-9	1.0162-9	1.2610-8	2.2719-9	1.4920-8	2.6880-9
NAOH		6.4140-9	1.423-12	1.4850-9	2.314-13	9.987-10	1.593-13
NA2SO4		2.2220-8	1.071-10	1.2150-8	2.144-11	8.8390-9	1.532-11
O		3.5190-9	1.979-11	1.5730-9	8.850-12	1.3300-9	7.479-12
OH		1.5463-6	5.5734-8	1.0340-6	3.7267-8	9.5058-7	3.4260-8
O2		6.7196-2	6.7181-2	6.7180-2	6.7144-2	6.7176-2	6.7136-2
O3		1.922-12	1.016-13	4.296-12	2.269-13	5.082-12	2.684-13
SO2		3.6405-4	2.4347-4	3.3202-4	1.6501-4	3.2260-4	1.4901-4
SO3		3.0808-5	1.5133-4	6.2820-5	2.2927-4	7.2220-5	2.4497-4
M, MOL WT		28.880	28.882	28.880	28.883	28.880	28.883
PHASE FRACTION	1.0000	0	1.0000	0	1.0000	0	1.0000
SOLUTION 2							
NAOH(L)		5.3139-6	6.2416-8	6.1536-6	5.0737-8	5.7922-6	4.9089-8
NA2SO3(S)		0.000	0	8.657-12	0.000	0	3.878-12
NA2SO3(L)		1.2020-9	0.000	0	1.4700-9	0.000	0
NA2SO4(I)		0.000000	9.5533-1	0.000000	9.5637-1	0.000000	9.5650-1
NA2SO4(L)		3.3446-1	0.000000	9.1453-1	0.000000	9.3150-1	0.000000
NA2V206(L)		6.6180-1	3.0516-2	8.3774-2	9.6759-3	6.6383-2	6.9623-3
NA4V207(S)		1.6410-4	1.3600-8	5.5700-6	5.699-10	2.7930-6	2.742-10
NA6V208(S)		1.981-10	0.000	0	1.804-12	0.000	0
V203(S)		1.0990-8	2.082-10	1.0380-9	9.999-11	7.687-10	7.687-11
V205(L)		3.5659-3	1.4152-2	1.6831-3	3.3956-2	2.1074-3	3.6543-2
M, MOL WT		209.59	145.71	150.63	144.38	148.88	144.20
PHASE FRACTION	1.8489-9	2.7550-8	1.4398-8	2.8205-8	1.7966-8	2.8297-8	2.0752-8
PURE SPECIES PHASE FRACTIONS (IF ANY)							
ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL							
SOLUTION 1							
C	CH	CH2	CH20	CH202	CH3	CH20H	CH30
CN	CN2	CNN	COS	CS	CS2	C2	C2H
C2H4	C2H402	C2H404	C2H5	C2H6	C2H3C2H3	C2H50H	C2H30CH3
C2O	C3	C3H60	M-C3H7	I-C3H7	C3H8	1-C3H70H	C3H2
N-C4H10	I-C4H10	C4H2	C5	C6H5	C6H50	C6H6	C6H50H
N-C8H18	I-C8H18	O-C12H17	C12H10	HCN	HCO	HNC0	H2N2
NCO	NH	NH2	NH3	N2H4	N2O4	N2O5	N3
NAH	NA0	NA2	NA2C2N2	NA20	NA2O2H2	S	SH
S2	S20	S8	V	VN	VO	VO2	
SOLUTION 2							
NAOH(A)	NA2O(C)	NA2O(A)	NA2O(L)	NA2SO4(IV)	NA2V206(S)	NA6V208(L)	V203(L)

OBSCURE SPECIES

CASE NO. 8701 331 1.0% SULFUR, 10 NA, 0.1 V PPM TIME = 0.536 SEC  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

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SOLUTION 1

AR 8.8043-3 8.8048-3 8.8044-3 8.8052-3 8.8045-3 8.8052-3 8.8045-3 8.8053-3 8.8046-3 8.8054-3  
 CO 3.0470-9 9.383-12 1.3630-9 4.198-12 1.1520-9 3.548-12 9.638-10 2.969-12 7.870-10 2.424-12  
 CO2 9.0029-2 9.0035-2 9.0031-2 9.0038-2 9.0031-2 9.0039-2 9.0032-2 9.0040-2 9.0032-2 9.0041-2  
 H 5.830-12 4.799-15 1.744-12 1.435-15 1.355-12 1.115-15 1.037-12 8.536-16 7.650-13 6.298-16  
 HNO 1.514-12 1.651-14 2.265-12 2.468-14 2.463-12 2.684-14 2.693-12 2.935-14 2.980-12 3.248-14  
 HNO2 4.1475-9 1.6158-9 1.3866-8 5.4006-9 1.7845-8 6.7503-9 2.3317-8 9.0813-9 3.1602-8 1.2308-8  
 HNO3 1.222-11 1.528-11 9.133-11 1.142-10 1.391-10 1.739-10 2.172-10 2.715-10 3.605-10 4.506-10  
 H2O 1.2030-8 9.760-10 1.7980-8 1.4590-9 1.9580-8 1.5870-9 2.1380-8 1.7350-9 2.3660-8 1.9190-9  
 H2 2.5750-9 1.594-11 1.1520-9 7.132-12 9.736-10 6.028-12 8.146-10 5.044-12 6.651-10 4.118-12  
 H2O 9.6171-2 9.6177-2 9.6173-2 9.6181-2 9.6173-2 9.6181-2 9.6174-2 9.6182-2 9.6175-2 9.6182-2  
 H2O2 4.812-10 5.480-11 1.0760-9 1.225-10 1.2730-9 1.449-10 1.5220-9 1.732-10 1.8630-9 2.121-10  
 H2SO4 2.6991-9 8.1422-8 2.7519-8 6.1681-7 4.4291-8 9.2264-7 7.3010-8 1.4031-6 1.2803-7 2.2388-6  
 N 9.5128-5 1.4918-5 9.5118-5 1.4915-5 9.5115-5 1.4914-5 9.5111-5 1.4913-5 9.5106-5 1.4912-5  
 N02 1.0155-6 5.2639-7 2.2702-6 1.1764-6 2.6860-6 1.3918-6 3.2101-6 1.6633-6 3.9311-6 2.0369-6  
 N03 1.282-13 2.831-14 6.407-13 1.414-13 8.969-13 1.980-13 1.281-12 2.827-13 1.921-12 4.240-13  
 N2 7.3731-1 7.3734-1 7.3732-1 7.3742-1 7.3732-1 7.3743-1 7.3733-1 7.3743-1 7.3733-1 7.3744-1  
 H2O 5.6401-9 1.0163-9 1.2610-8 2.2719-9 1.4920-8 2.6880-9 1.7832-8 3.2126-9 2.1839-8 3.9344-9  
 NA 1.431-12 4.644-18 6.000-14 2.257-19 3.106-14 1.212-19 1.549-14 6.292-20 7.047-15 3.001-20  
 NAOH 1.1060-8 1.453-12 1.5500-9 2.361-13 1.0330-9 1.632-13 6.730-10 1.107-13 4.150-10 7.155-14  
 NA2SO4 6.6020-8 1.116-10 2.232-11 9.4450-9 1.594-11 6.6120-9 1.116-11 4.4080-9 7.440-12  
 O 3.5190-9 1.979-11 1.5730-9 8.850-12 1.3300-9 7.479-12 1.1120-9 6.257-12 9.083-10 5.109-12  
 OH 1.5463-6 5.5734-8 1.0340-6 3.7267-8 9.5058-7 3.4260-8 8.6947-7 3.1334-8 7.8564-7 2.8315-8  
 O2 6.7197-2 6.7182-2 6.7181-2 6.7145-2 6.7177-2 6.7137-2 6.7171-2 6.7130-2 6.7164-2 6.7121-2  
 O3 1.972-12 1.016-13 4.296-12 2.269-13 5.082-12 2.684-13 6.074-12 3.208-13 7.438-12 3.928-13  
 SO2 3.6382-4 2.4332-4 3.3181-4 1.6490-4 3.2240-4 1.4892-4 3.1127-4 1.3264-4 2.9713-4 1.1521-4  
 SO3 3.0789-5 1.5124-4 6.2781-5 2.2913-4 7.2175-5 2.4481-4 8.3283-5 2.6061-4 9.7363-5 2.7721-4  
 M, MOL WT 28.880 28.882 28.880 28.883 28.880 28.883 28.881 28.883 28.881 28.883  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

SOLUTION 2

NAOH(L) 9.1630-6 6.3734-8 6.4213-6 5.1781-8 5.9891-6 5.0095-8 5.5756-6 4.8553-8 5.1568-6 4.7077-8  
 NA2SO3(S) 0.000 0 9.023-12 0.000 0 4.036-12 0.000 0 3.411-12 0.000 0 2.854-12 0.000 0 2.331-12  
 NA2SO3(L) 3.5720-9 0.000 0 1.6000-9 0.000 0 1.3320-9 0.000 0 1.1310-9 0.000 0 9.239-10 0.000 0  
 NA2SO4(I) 0.000000 9.7549-1 0.000000 9.7550-1 0.000000 9.7550-1 0.000000 9.7551-1 0.000000 9.7551-1  
 NA2SO4(L) 9.7387-1 0.000000 9.7524-1 0.000000 9.7531-1 0.000000 9.7534-1 0.000000 9.7541-1 0.000000  
 NA2V206(L) 6.1029-3 3.1204-3 4.6702-3 1.0294-3 4.5482-3 7.4445-4 4.4138-3 5.1882-4 4.2262-3 3.3974-4  
 NA4V207(S) 4.4990-6 1.4500-9 3.3810-7 6.315-11 2.0460-7 3.053-11 1.2050-7 1.399-11 6.5780-8 5.742-12  
 NA6V208(S) 1.615-11 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0  
 V203(S) 3.410-11 2.042-11 5.314-11 1.021-11 5.950-11 7.892-12 6.663-11 5.856-12 7.459-11 4.079-12  
 V205(L) 1.1059-5 1.3880-3 8.6165-5 3.4683-3 1.3505-4 3.7519-3 2.1602-4 3.9764-3 3.6271-4 4.1546-3  
 M, MOL WT 142.66 142.41 142.52 142.28 142.51 142.26 142.49 142.25 142.48 142.24  
 PHASE FRACTION 2.0111-7 2.7294-7 2.5869-7 2.7361-7 2.6274-7 2.7370-7 2.6577-7 2.7377-7 2.6815-7 2.7392-7

PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH2OH	CH30	CH4	CH
CN	CN2	CNN	COS	CS	CS2	C2	C2H	C2Z	C2
C2H4	C2H402	C2H404	C2H5	C2H6	C3H2C3H3	C2H5OH	C3H3C3H3	C2N	C2
C2O	C3	C3H60	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	C5	C6H5	C6H50	C6H6	C6H5OH	C7H8	C8
N-C8H18	I-C8H18	O-C12H19	C12H10	HCO	HCO	HCO	H2N2	H2S	N
NO	NH	NH2	NH3	N2H4	N2O4	N2O5	N3	NACN	NA
NA2	NA2	NA2C2N2	NA2O	NA2O2H2	S	SH	SH	SO	S2
S2O	S8	V	VN	VO	VO2				

SOLUTION 2

NAOH(A)	NA2O(C)	NA2O(A)	NA2O(L)	NA2SO4(IV)	NA2V206(S)	NA6V208(L)	V203(L)	V205(S)	
PURE SPECIES									
C(GR)	C7H8(L)	CBH18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	N2H8SO4(S)	NA(S)	NA
NACN(S)	NACN(L)	NA2O2(S)	NA2CO3(1)	NA2CO3(2)	NA2CO3(L)	NA2O2(A)	NA2O2(B)	NA2S(1)	NA
NA2S(L)	S(S)	S(L)	V(S)	V(L)	NAV308(S)	NA2V12031(S)	NA2V12031(L)	V0(S)	VO
V02(S)	V02(S)	V02(L)							



CASE NO. 8701 232 1.0% SULFUR, 1.0 NA, 1.0 V PPM TIME = 0.733 SEC  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

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SOLUTION 1

AR 8.8043-3 8.8048-3 8.8044-3 8.8052-3 8.8045-3 8.8052-3 8.8045-3 8.8053-3 8.8046-3 8.8054-3  
 CO 3.0470-9 9.383-12 1.3630-9 4.198-12 1.1520-9 3.548-12 9.638-10 2.968-12 7.870-10 2.424-12  
 CO2 9.0030-2 9.0035-2 9.0031-2 9.0039-2 9.0032-2 9.0040-2 9.0032-2 9.0041-2 9.0033-2 9.0041-2  
 H 5.830-12 4.799-15 1.744-12 1.435-15 1.355-12 1.115-15 1.037-12 8.536-16 7.650-13 6.298-16  
 HNO 1.514-12 1.651-14 2.265-12 2.468-14 2.453-12 2.684-14 2.693-12 2.935-14 2.980-12 3.249-14  
 HNO2 4.1475-9 1.6158-9 1.3866-8 5.4006-9 1.7845-8 6.9503-9 2.3317-8 9.0812-9 3.1601-8 1.2308-8  
 HNO3 1.222-11 1.528-11 9.133-11 1.142-10 1.391-10 1.739-10 2.172-10 2.715-10 3.605-10 4.506-10  
 HO2 1.203-8 9.760-10 1.7980-8 1.4590-9 1.9560-8 1.5870-9 2.1380-8 1.7350-9 2.3860-8 1.9190-9  
 H2 2.5750-9 1.594-11 1.1520-9 7.132-12 9.736-10 6.028-12 8.146-10 5.044-12 6.651-10 4.119-12  
 H2O 9.6172-2 9.6178-2 9.6173-2 9.6181-2 9.6174-2 9.6182-2 9.6174-2 9.6182-2 9.6175-2 9.6182-2  
 H2O2 4.812-10 5.480-11 1.0760-9 1.225-10 1.2730-9 1.449-10 1.5220-9 1.732-10 1.8630-9 2.121-10  
 H2SO4 2.7008-9 8.1474-8 2.7537-8 6.1720-7 4.4320-8 9.2323-7 7.3058-8 1.4040-8 1.2812-7 2.2402-6  
 NO 9.5128-5 1.4918-5 9.5117-5 1.4914-5 9.5114-5 1.4914-5 9.5110-5 1.4913-5 9.5105-5 1.4912-5  
 NO2 1.0155-6 5.2638-7 2.2702-6 1.1764-6 2.6859-6 1.3918-6 3.2100-6 1.6633-6 3.9310-6 2.0369-6  
 NO3 1.282-13 2.831-14 6.407-13 1.414-13 8.969-13 1.980-13 1.281-12 2.827-13 1.921-12 4.240-13  
 N2 7.3731-1 7.3739-1 7.3732-1 7.3742-1 7.3732-1 7.3743-1 7.3732-1 7.3743-1 7.3733-1 7.3744-1  
 N2O 5.6400-9 1.0162-9 1.2610-8 2.2719-9 1.4970-8 2.6880-9 1.7832-8 3.2126-9 2.1839-8 3.9344-9  
 NaOH 4.4220-9 1.146-12 1.0180-9 1.939-13 7.089-10 1.345-13 4.784-10 9.152-14 3.040-10 5.928-14  
 Na2S04 1.0560-8 6.943-11 5.7020-9 1.506-11 4.4530-9 1.084-11 3.3430-9 7.633-12 2.3680-9 5.110-12  
 O 3.5190-9 1.979-11 1.5730-9 8.850-12 1.3300-9 7.479-12 1.1120-9 6.257-12 9.083-10 5.109-12  
 OH 1.5463-6 5.5734-8 1.0340-8 3.7267-8 9.5058-7 3.4260-8 8.6947-7 3.1338-8 7.8564-7 2.8315-8  
 O2 6.7197-2 6.7181-2 6.7180-2 6.7144-2 6.7176-2 6.7136-2 6.7170-2 6.7129-2 6.7163-2 6.7120-2  
 O3 1.922-12 1.016-13 4.296-12 2.269-13 5.082-12 2.684-13 6.074-12 3.208-13 7.438-12 3.928-13  
 SO2 3.6406-4 2.4347-4 3.3203-4 1.6501-4 3.2261-4 1.4901-4 3.1147-4 1.3273-4 2.9733-4 1.1528-4  
 SO3 3.0809-5 1.5133-4 6.2822-5 2.2927-4 7.2222-5 2.4497-4 8.3337-5 2.6078-4 9.7426-5 2.7739-4  
 M, MOLE WT 28.880 28.882 28.880 28.883 28.880 28.883 28.881 28.883 28.881 28.883  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

SOLUTION 2

NaOH(L) 3.6636-6 5.0256-8 4.2158-6 4.2527-8 4.1113-6 4.1299-8 3.9632-6 4.0141-8 3.7781-6 3.9004-8  
 Na2S03(S) 0.000 0 5.614-12 0.000 0 2.724-12 0.000 0 2.320-12 0.000 0 1.952-12 0.000 0 1.601-12  
 Na2S03(L) 5.714-10 0.000 0 6.900-10 0.000 0 6.376-10 0.000 0 5.720-10 0.000 0 4.962-10 0.000 0  
 Na2S04(I) 0.000000 6.1934-1 0.000000 6.7190-1 0.000000 6.7702-1 0.000000 6.8085-1 0.000000 6.8377-1  
 Na2S04(L) 1.5898-1 0.000000 4.2925-1 0.000000 4.6932-1 0.000000 5.0324-1 0.000000 5.3485-1 0.000000  
 Na2V204(L) 8.3149-1 2.2190-1 5.4731-1 5.4729-2 4.9921-1 3.8380-2 4.5288-1 2.6131-2 4.0120-1 1.6807-2  
 Na4V207(S) 9.7990-5 6.4120-8 1.7080-5 2.2650-9 1.0580-5 1.0700-9 6.2450-6 4.817-10 3.3520-6 1.950-10  
 Na6V208(S) 5.624-11 0.000 0 2.596-12 0.000 0 1.073-12 0.000 0 0.000 0 0.000 0 0.000 0  
 V203(S) 2.9060-8 2.3360-9 1.4450-8 8.050-10 1.3860-8 5.987-10 1.3330-8 4.315-10 1.3190-8 2.940-10  
 V203(L) 9.4255-3 1.5874-1 2.3427-2 2.7338-1 3.1456-2 2.8460-1 4.3870-2 2.9302-1 6.4147-2 2.9942-1  
 M, MOLE WT 227.09 170.96 198.70 158.50 194.12 157.28 189.90 156.37 185.44 155.68  
 PHASE FRACTION 1.4631-8 3.2329-8 2.1560-8 3.7507-8 2.3188-8 3.8102-8 2.4771-8 3.8560-8 2.6443-8 3.8917-8

PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH20H	CH30	CH4	CH
CN	CN2	CN0	C0S	C02	C2	C2H	C2H2	C2	
C2H4	C2H402	C2H404	C2H5	C2H6	CX3N2CH3	C2HS0H	C2SOCH3	C2N	C2
C20	C3	C3H0	N-C3H7	I-C3H7	C3H8	1-C3H7OH	C3D2	C4	C4
N-C4H10	I-C4H10	C4H2	C5	C6H5	C6H50	C6H6	C6HS0H	C7H8	C8
N-C8H18	I-C8H18	O-C12H9	C12H10	HCO	HCO	HCO	H2N2	H2S	N
NaO	NH	NH2	NH3	NH4	N204	N205	N3	NA	NA
NaH	NaO	Na2	Na2C2N2	Na20	Na202H2	S	SH	SN	SD
S2	S20	S8	V	VN	VO	VO2			

SOLUTION 2

NaOH(A)	Na2O(C)	Na2O(A)	Na2O(L)	Na2S04(IV)	Na2V206(S)	Na6V208(L)	V203(L)	V203(S)
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PURE SPECIES

C(1R)	C7H8(L)	C8H18(L)	H20(S)	H20(L)	H2S04(L)	VN(S)	N2HS04(S)	NA(S)	NA
NaCN(S)	NaCN(L)	NaO2(S)	Na2C03(1)	Na2C03(2)	Na2C03(L)	Na2O2(A)	Na2O2(B)	Na2S(1)	NA
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaVS08(S)	Na2V12031(S)	Na2V12031(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

CASE NO. 8701 332 1.0Z SULFUR, 10 NA, 1.0 V PPM singular matrix, iteration 29 variable 7

P, ATM 1.0000 1.0000

T, DEG K 1172.0 977.0

SOLUTION 1

AR 8.8043-3 8.8048-3

CO 3.0470-9 9.333-12

CO2 9.0029-2 9.0035-2

H 5.830-12 4.799-15

HNO 1.514-12 1.651-14

HNO2 4.1475-9 1.6158-9

HNO3 1.222-11 1.528-11

H2 2.5750-9 1.594-11

H2O 9.6171-2 9.6177-2

H2O2 4.812-10 5.480-11

H2SO4 2.6992-9 8.1423-8

NO 9.5129-5 1.4918-5

NO2 1.0155-6 5.2639-7

N2 7.3731-1 7.3739-1

N2O 5.6401-9 1.0163-9

NA 1.392-12 4.550-18

NAOH 1.0760-8 1.424-12

NA2SO4 6.2430-8 1.071-10

O 3.5190-9 1.979-11

OH 1.5463-6 5.5734-8

O2 6.7198-2 6.7182-2

O3 1.922-12 1.016-13

SO2 3.6383-4 2.4332-4

SO3 3.0790-5 1.5124-4

M, MOL WT 28.880 28.882

PHASE FRACTION 1.0000 0 1.0000 0

SOLUTION 2

NAOH(L) 8.9107-6 6.2440-8

NA2SO3(S) 0.000 0 8.660-12

NA2SO3(L) 3.3780-9 0.000000

NA2SO4(I) 0.000000 9.5549-1

NA2SO4(L) 9.3993-1 0.000000

NA2V206(L) 5.9908-2 3.0416-2

NA4V207(S) 4.1765-5 1.3566-8

NA6V208(S) 1.418-10 0.000 0

V203(S) 3.539-10 2.074-10

V205(L) 1.1479-4 1.4095-2

M, MOL WT 148.15 145.70

PHASE FRACTION 2.0486-7 2.7646-7

PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH20H	CH30	CH4	CH
CN	CN2	CNN	COS	CS	CS2	C2	C2H	C2H2	C2
C2H4	C2H402	C2H404	C2H5	C2H6	C2H50C2H3	C2H50H	C2H50C2H3	C2N	C2
C2D	C3	C3H60	N-C3H7	I-C3H7	C3H8	I-C3H70H	C3D2	C4	C4
N-C4H10	I-C4H10	C4N2	C5	C6H5	C6H50	C6H6	C6H50H	C7H8	C8
N-C8H18	I-C8H18	O-C12H9	C12H10	HON	HCO	HNO	H2N2	H2S	N
NO	NH	NH2	NH3	N03	N2H4	N2O4	N2O5	N3	NA
NAH	NA0	NA2	NA2C2N2	NA2D	NA2O2H2	S	SH	SN	SD
S2	S20	S8	V	VN	VO	V02			

SOLUTION 2

NAOH(A)	NA2D(C)	NA2D(A)	NA2D(L)	NA2SO4(IV)	NA2V206(S)	NA6V208(L)	V203(L)	V205(S)
---------	---------	---------	---------	------------	------------	------------	---------	---------

PURE SPECIES

C(G)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	NA2HSO4(S)	NA(S)	NA
NACN(S)	NAOH(L)	NA2(S)	NA2CO3(I)	NA2CO3(2)	NA2CO3(L)	NA2O2(A)	NA2O2(B)	NA2S(I)	NA
NA2S(L)	S(S)	S(L)	V(S)	V(L)	NAV308(S)	NA2V12031(S)	NA2V12031(L)	V0(S)	V0
V02(S)	V02(S)	V02(L)							

CASE NO. 8701 133 1.02 SULFUR, 0.1 NA, 10 V PPM TIME = 0.571 SEC  
 P, ATM 1.0000 1.0000 5.0000 5.0000 7.0000 7.0000 10.000 10.000 15.000 15.000  
 T, DEG K 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0 1172.0 977.0

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SOLUTION 1

AR 8.8043-3 8.8043-3 8.8044-3 8.8052-3 8.8045-3 8.8052-3 8.8045-3 8.8053-3 8.8045-3 8.8054-3  
 CO 3.0470-9 9.383-12 1.3630-9 4.198-12 1.1520-9 3.548-12 9.638-10 2.969-12 7.870-10 2.424-12  
 CO2 9.0029-2 9.0035-2 9.0031-2 9.0032-2 9.0031-2 9.0039-2 9.0032-2 9.0040-2 9.0032-2 9.0041-2  
 H 5.930-12 4.799-15 1.744-12 1.435-15 1.355-12 1.115-15 1.037-12 8.536-16 7.650-13 6.298-16  
 HNO 1.514-12 1.651-14 2.285-12 2.468-14 2.483-12 2.684-14 2.693-12 2.935-14 2.990-12 3.249-14  
 HNO2 4.1475-9 1.6158-9 1.3866-8 5.4006-9 1.7345-8 6.9503-9 2.3317-8 9.0813-9 3.1602-8 1.2308-8  
 HNO3 1.222-11 1.529-11 9.133-11 1.142-10 1.391-10 1.737-10 2.172-10 2.715-10 3.605-10 4.506-10  
 H2 1.2030-3 9.750-10 1.7930-2 1.4590-9 1.9560-9 1.5870-9 2.1380-8 1.7350-9 2.3660-9 1.9190-9  
 H2 2.5750-9 1.594-11 1.1520-9 7.132-12 9.736-10 6.028-12 8.146-10 5.044-12 6.651-10 4.118-12  
 H2O 9.6171-2 9.6177-2 9.6173-2 9.6181-2 9.6173-2 9.6181-2 9.6174-2 9.6182-2 9.6175-2 9.6182-2  
 H2O2 4.812-10 5.480-11 1.0760-9 1.225-10 1.2730-9 1.449-10 1.5220-9 1.732-10 1.8630-9 2.121-10  
 H2SO4 2.7009-9 8.1477-8 2.7337-8 6.1723-7 4.4321-8 9.2327-7 7.3060-8 1.4041-6 1.2812-7 2.2403-6  
 NO 9.5128-5 1.4918-5 9.5118-5 1.4915-5 9.5115-5 1.4914-5 9.5111-5 1.4913-5 9.5106-5 1.4912-5  
 NO2 1.0155-6 5.2639-7 2.2702-6 1.1764-6 2.6860-6 1.3918-6 3.2101-6 1.6633-6 3.9311-6 2.0369-6  
 NO3 1.282-13 2.831-14 6.407-13 1.414-13 8.969-13 1.980-13 1.281-12 2.827-13 1.921-12 4.240-13  
 N2 7.3731-1 7.3739-1 7.3732-1 7.3742-1 7.3732-1 7.3743-1 7.3733-1 7.3743-1 7.3733-1 7.3744-1  
 N2O 5.6401-9 1.0163-9 1.2610-8 2.2719-9 1.4920-8 2.6880-9 1.7832-8 3.2126-9 2.1839-8 3.9344-9  
 NaOH 7.030-11 1.204-13 3.127-11 3.072-14 2.629-11 2.204-14 2.179-11 1.539-14 1.748-11 1.016-14  
 Na2SO4 2.669-12 7.692-13 5.384-12 3.782-13 6.124-12 2.916-13 6.935-12 2.160-13 7.826-12 1.502-13  
 O 3.5190-9 1.979-11 1.5730-9 8.850-12 1.3300-9 7.479-12 1.1120-9 6.257-12 9.083-10 5.109-12  
 OH 1.5463-6 5.5734-8 1.0340-6 3.7267-8 9.5058-7 3.4260-8 8.6947-7 3.1336-7 7.8564-7 2.8315-8  
 O2 6.7197-2 6.7182-2 6.7181-2 6.7145-2 6.7177-2 6.7137-2 6.7171-2 6.7129-2 6.7164-2 6.7121-2  
 O3 1.922-12 1.016-13 4.294-12 2.269-13 5.062-12 2.684-13 6.074-12 3.209-13 7.439-12 3.929-13  
 SO2 3.6407-4 2.4348-4 3.3204-4 1.6502-4 3.2262-4 1.4902-4 3.1148-4 1.3273-4 2.9734-4 1.1529-4  
 SO3 3.0810-5 1.5134-4 6.2824-5 2.2929-4 7.2224-5 2.4498-4 8.3340-5 2.6079-4 9.7430-5 2.7740-4  
 M, MOLE WT 28.880 28.882 28.880 28.883 28.880 28.883 28.881 28.883 28.881 28.883  
 PHASE FRACTION 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0 1.0000 0

SOLUTION 2

NaOH(L) 5.8244-8 5.2894-9 1.2954-7 6.7381-9 1.5245-7 6.7725-9 1.8052-7 6.7517-9 2.1721-7 6.6869-9  
 Na2SO3(L) 0.000 0 0.000 0 0.000 0 0.000 0 1.187-12 0.000 0 1.640-12 0.000 0  
 Na2SO4(I) 0.000000 6.8613-3 0.000000 1.6868-2 0.000000 1.8207-2 0.000000 1.9263-2 0.000000 2.0099-2  
 Na2SO4(L) 4.0184-5 0.000000 4.0530-4 0.000000 6.4534-4 0.000000 1.0441-3 0.000000 1.7672-3 0.000000  
 Na2V2O6(L) 2.1810-2 1.5145-2 2.1573-2 4.9163-3 2.1342-2 3.5476-3 2.0946-2 2.4682-3 2.0217-2 1.6140-3  
 Na4V2O7(S) 6.496-10 4.847-11 6.357-10 5.107-12 6.221-10 2.859-12 5.993-10 1.287-12 5.583-10 0.000 0  
 V2O3(S) 3.0160-6 1.4390-8 6.0320-7 2.8800-9 4.3090-7 2.0580-9 3.0160-7 1.4410-9 2.0110-7 9.606-10  
 V2O5(L) 9.7815-1 9.7799-1 9.7802-1 9.7822-1 9.7801-1 9.7825-1 9.7801-1 9.7827-1 9.7802-1 9.7829-1  
 M, MOLE WT 183.23 182.55 183.20 181.51 183.18 181.37 183.14 181.27 183.06 181.18  
 PHASE FRACTION 1.2305-7 1.2391-7 1.2310-7 1.2517-7 1.2313-7 1.2534-7 1.2318-7 1.2548-7 1.2327-7 1.2559-7

PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH20	CH202	CH3	CH2OH	CH3O	CH4	CH
CN	CN2	CNH	COS	CS	C5	C2	CZH	C2H2	C2
C2H4	C2H402	C2H404	C2H5	C2H6	C3H2CH3	C2H5OH	C3H3CH3	C2N	C2
C2O	C3	C3H60	H-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
H-C4H10	I-C4H10	C4H2	CS	C4H5	C4H5O	C4H6	C4H5OH	C7H8	C8
H-C8H18	I-C8H18	O-C12H9	C12H10	HCO	HCO	HCO	H2O2	H2S	N
NO	NH	NH2	NH3	N2H4	N2O4	N2O5	N3	NA	NA
NAH	NaO	Na2	Na2C2H2	Na2O	Na2O2H2	S	SH	SN	SO
S2	S2O	S8	V	VN	VO	VO2			

SOLUTION 2

NaOH(A) Na2O(C) Na2O(A) Na2O(L) Na2SO3(S) Na2SO4(IV) Na2V2O6(S) Na4V2O8(S) Na4V2O8(L) V2

V2O5(S)

PURE SPECIES

C(GR)	C7H8(L)	CBH18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	N2HBSO4(S)	Na(S)	Na
NaCN(S)	NaCN(L)	NaO2(S)	Na2O3(S)	Na2O3(L)	Na2O2(A)	Na2O2(B)	Na2S(L)	Na	Na
Na2S(L)	S(S)	S(L)	V(S)	V(L)	NaV3O8(S)	Na2V12O31(S)	Na2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							



CASE NO. 8701 333 1.0% SULFUR, 10 NA, 10 V PPM singular matrix, iteration 27 variable 1

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P, ATM 1.0000 1.0000

T, DEG K 1172.0 977.0

SOLUTION 1

AR 8.8043-3 8.8048-3

CO 3.0470-9 3.383-12

CO2 9.0028-2 9.0034-2

H 5.830-12 4.799-15

HNO 1.514-12 1.651-14

HNO2 4.1176-9 1.6158-9

HNO3 1.222-11 1.528-11

H2 1.2030-8 9.760-10

H2 2.5750-9 1.594-11

H2O 9.6170-2 9.6177-2

H2O2 4.812-10 5.480-11

H2SO4 2.6999-9 8.1435-8

HO 9.5129-5 1.4919-5

HO2 1.0153-6 5.2640-7

H2 7.3731-1 7.3739-1

H2O 5.6401-9 1.0163-9

NAOH 7.6960-9 1.147-12

NA2SO4 3.1970-4 6.951-11

O 3.5190-9 1.979-11

OH 1.5463-3 5.5734-8

O2 6.7198-2 6.7183-2

O3 1.922-12 1.016-13

SO2 3.6393-4 2.4336-4

SO3 3.0799-5 1.5125-4

M, MOL WT 28.880 28.882

PHASE FRACTION 1.0000 0 1.0000 0

SOLUTION 2

NAOH(L) 6.3758-6 5.0295-8

NA2SO3(S) 0.000 0 5.620-12

NA2SO3(L) 1.7299-9 0.000000

NA2SO4(I) 0.000000 6.2005-1

NA2SO4(L) 4.8135-1 0.000000

NA2V2O6(L) 5.1653-1 2.2165-1

NA4V2O7(S) 1.8436-4 6.4143-8

NA6V2O8(S) 3.205-10 0.000 0

V2O3(S) 5.9600-9 2.3294-9

V2O5(L) 1.9332-3 1.5830-1

M, MOL WT 194.74 170.91

PHASE FRACTION 2.3725-7 3.2387-7

PURE SPECIES PHASE FRACTIONS (IF ANY)

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN 0.10000E-11 FOR ALL ASSIGNED CONDITIONS

SOLUTION 1

C	CH	CH2	CH2O	CH2O2	CH3	CH2OH	CH3O	CH4	CH
CH	CH2	CHN	CO	CS	C2	C2H	C2H2	C2	
C2H	C2H2	C2H4	C2H4	C2H5	C2H6	C2H2C2H3	C2H5O	C2H	C2
C2O	C3	C3H6	N-C3H7	I-C3H7	C3H8	I-C3H7OH	C3O2	C4	C4
N-C4H10	I-C4H10	C4H2	C5	C4H5	C4H6	C4H5OH	C7H8	C8	
N-C3H18	I-C3H18	O-C12H27	C12H10	HCO	HCO	H2O2	H2S	N	
NCO	NH	NH2	NH3	NH3	N2H4	N2O4	N2S	N	NA
NAOH	NAH	NAO	NA2	NA2C2H2	NA2O	NA2O2H2	S	SH	SN
SO	S2	S2O	S8	V	VN	VO	VO2		

SOLUTION 2

NAOH(A) NA2O(C) NA2O(A) NA2O(L) NA2SO4(IV) NA2V2O6(S) NA6V2O8(L) V2O3(L) V2O5(S)

PURE SPECIES

C(GR)	C7H8(L)	C8H18(L)	H2O(S)	H2O(L)	H2SO4(L)	VN(S)	N2HBSO4(S)	NA(S)	NA
NAOH(S)	NAOH(L)	NAO2(S)	NA2CO3(I)	NA2CO3(2)	NA2CO3(L)	NA2O2(A)	NA2O2(B)	NA2S(I)	NA
NA2S(L)	S(I)	S(L)	V(S)	V(L)	NA2SO8(S)	NA2V12O31(S)	NA2V12O31(L)	VO(S)	VO
VO2(S)	VO2(S)	VO2(L)							

STOP

Appendix B. CFBL calculations of  $\text{Na}_2\text{SO}_4$  deposition rates for selected fuel impurity levels from Table 2. Calculations are repeated for two different wall temperatures, 977 and 1172K.

CASE NO. 8701 131 0.1 ppm Na, 1%S, 0.1 ppm V

V1ROP1HT

## - - INPUT PARAMETERS - -

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 1172.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULANCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39893E+01	0.10853E+01	0.50180E-08	0.13280E-08	0.45016E-01	1.02268	0.89010E-03
2	0.35112E+01	0.36321E+01	0.85843E+00	0.41340E-09	0.00000E+00	-0.15846E-01	0.99210	0.10953E-03
3	0.17005E+01	0.48542E+01	0.17725E+01	0.14160E-16	0.95190E-09	0.17019E+00	1.08751	-0.29915E-03
6	0.23382E+01	0.42736E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.92532E-01	1.04698	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-08	0.323180E-08	0.394772E-03	0.394881E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 1.65482E-11

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 3.92336E-07

Na-to-S molar flux ratio at the surface = 0.0001

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 7.00474E-04  
 ERROR (%) = -8.443E+01

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

NO. 8701 231 1.0 ppm Na, 1%S, 0.1 ppm V

V1ROP1HT

## - - INPUT PARAMETERS - -

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 1172.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULENCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
0.27773E+01	0.39893E+01	0.10853E+01	0.50180E-07	0.64140E-08	0.45016E-01	1.02268	0.10455E-01
0.35112E+01	0.36321E+01	0.85843E+00	0.41340E-08	0.00000E+00	-0.15846E-01	0.99210	0.10953E-02
0.17005E+01	0.48542E+01	0.17725E+01	0.14160E-14	0.22220E-07	0.17019E+00	1.08751	-0.69830E-02
0.23382E+01	0.42736E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.92532E-01	1.04698	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-07	0.508540E-07	0.394772E-03	0.394880E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 1.07891E-10

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 3.92381E-07

Na-to-S molar flux ratio at the surface = 0.0004

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 4.56697E-03  
 ERROR (%) = 1.488E+00

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

HOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

CASE NO. 8701 331 10 ppm Na, 1%S, 0.1 ppm V

V1ROP1HT

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## INPUT PARAMETERS

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19	TYPE = 0	
TO (K) = 1806.000	PO (ATM) = 1.068000	
TW (K) = 1172.000	PJ (ATM) = 1.000000	
Fuel/Air Mass Ratio (F) = 0.045380	OPTIONAL PARAMETERS	
Air Flow Rate (WA, G/SEC) = 2.94000	Nozzle Discharge Coef (DC) = 1.000000	
Dia. Cyl. Target (DIAW, CM) = 0.31800	SHAPE = 0.0000	DIV = 0.0000
Length (hgt) Target (LW, CM) = 3.81000	TURBULANCE	
Dia. Jet Nozzle (DJ, CM) = 6.03300	TURB = 0.0000	
Observed Deposition rate (WOBS, MG/HR) = 0.0045	TURIN = 0.0000 PERCENT	
FSORET? = T	TURL (CM) = 0.00000	

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39893E+01	0.10853E+01	0.50180E-06	0.11060E-07	0.45016E-01	1.02268	0.11656E+00
2	0.35112E+01	0.36321E+01	0.85843E+00	0.41340E-07	0.14310E-11	-0.15846E-01	0.99210	0.10952E-01
3	0.17005E+01	0.48542E+01	0.17725E+01	0.14160E-12	0.66020E-07	0.17019E+00	1.08751	-0.20748E-01
6	0.23382E+01	0.42736E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.92532E-01	1.04698	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-06	0.143101E-06	0.394762E-03	0.394675E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 2.52220E-09

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 3.93834E-07

Na-to-S molar flux ratio at the surface = 0.0089

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.06763E-01  
 ERROR (%) = 2.273E+03

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

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CASE NO. 8701 132 0.1 ppm Na, 1%S, 1.0 ppm V

V1ROP1HT

## -- INPUT PARAMETERS --

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 1172.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULENCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39893E+01	0.10853E+01	0.50180E-08	0.24180E-09	0.45016E-01	1.02268	0.11359E-02
2	0.35112E+01	0.36321E+01	0.85843E+00	0.41340E-09	0.00000E+00	-0.15846E-01	0.99210	0.10953E-03
3	0.17005E+01	0.48542E+01	0.17725E+01	0.14160E-16	0.31580E-10	0.17019E+00	1.08751	-0.99245E-05
5	0.23382E+01	0.42736E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.92532E-01	1.04698	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-08	0.304960E-09	0.394772E-03	0.394880E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 2.91878E-11

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 3.92340E-07

Na-to-S molar flux ratio at the surface = 0.0001

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.23550E-03  
 ERROR (%) = -7.254E+01

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

77

CASE NO. 8701 232 1.0 ppm Na, 1%S, 1.0 ppm V

V1ROP1HT

## INPUT PARAMETERS

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 1172.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULENCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39893E+01	0.10853E+01	0.50180E-07	0.44220E-08	0.45016E-01	1.02268	0.10905E-01
2	0.35112E+01	0.36321E+01	0.85843E+00	0.41340E-08	0.00000E+00	-0.15846E-01	0.99210	0.10953E-02
3	0.17005E+01	0.48542E+01	0.17725E+01	0.14160E-14	0.10560E-07	0.17019E+00	1.08751	-0.33186E-02
6	0.23382E+01	0.42736E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.92532E-01	1.04698	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-07	0.255420E-07	0.394772E-03	0.394880E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 2.05108E-10

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 3.92364E-07

Na-to-S molar flux ratio at the surface = 0.0007

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 8.68209E-03  
 ERROR (%) = 9.294E+01

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

78

CASE NO. 8701 332 10. ppm Na, 1% S, 1.0 ppm V

V1ROP1HT

## - - INPUT PARAMETERS - -

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 1172.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

OPTIONAL PARAMETERS  
 Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULENCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39893E+01	0.10853E+01	0.50180E-06	0.10760E-07	0.45016E-01	1.02268	0.11663E+00
2	0.35112E+01	0.36321E+01	0.85843E+00	0.41340E-07	0.13920E-11	-0.15846E-01	0.99210	0.10952E-01
3	0.17005E+01	0.48542E+01	0.17725E+01	0.14160E-12	0.62430E-07	0.17019E+00	1.08751	-0.19620E-01
6	0.23382E+01	0.42736E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.92532E-01	1.04698	0.00000E+00

YNAJ            YNAW            YSJ            YSW  
 0.543140E-06    0.135621E-06    0.394762E-03    0.394682E-03

Average Molec. Wt.= 28.81275  
 Turbulence factor = 1.00000 .  
 Re(EFF) = 57.533  
 Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 2.55046E-09  
 Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 3.93775E-07  
 Na-to-S molar flux ratio at the surface = 0.0090

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.07959E-01  
 ERROR (%) = 2.299E+03

GM = 1.26949  
 TJ (K) = 1780.95  
 PR = 0.690190  
 MOLE FRACTIONS  
 X(N2) = 0.755099  
 X(O2) = 0.065770  
 X(H2O) = 0.089565  
 X(CO2) = 0.089565

RHOJ(G/CM\*\*3)    UJ(CM/S)    ETAMIX(POISE)    LAMIX(CAL/CM/K/S)    CMIX(CAL/G/S)  
 0.197159E-03    0.545317E+03    0.594261E-03    0.279215E-03    0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

79

CASE NO: 8701 133 0.1 ppm Na, 1%S, 10. ppm V

V1ROP1HT

## -- INPUT PARAMETERS --

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 1172.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

OPTIONAL PARAMETERS  
 Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULANCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39893E+01	0.10853E+01	0.50180E-08	0.70300E-10	0.45016E-01	1.02268	0.11747E-02
2	0.35112E+01	0.36321E+01	0.85843E+00	0.41340E-09	0.00000E+00	-0.15846E-01	0.99210	0.10953E-03
3	0.17005E+01	0.48542E+01	0.17725E+01	0.14160E-16	0.26690E-11	0.17019E+00	1.08751	-0.83877E-06
5	0.23382E+01	0.42736E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.92532E-01	1.04698	0.00000E+00

YNAJ            YNAW            YSJ            YSW  
 0.543140E-08    0.756380E-10    0.394762E-03    0.394880E-03

Average Molec. Wt.= 28.81275  
 Turbulence factor = 1.00000  
 Re(EFF) = 57.533  
 Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.03192E-11  
 Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 3.92260E-07  
 Na-to-S molar flux ratio at the surface = 0.0001

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.28339E-03  
 ERROR (%) = -7.148E+01

GM = 1.26949  
 TJ (K) = 1780.95  
 PR = 0.690190  
 MOLE FRACTIONS  
 X(N2) = 0.755099  
 X(O2) = 0.065770  
 X(H2O) = 0.089565  
 X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

CASE NO: 8701 233 1.0 ppm Na, 1%S, 10. ppm V

V1R0P1HT

## -- INPUT PARAMETERS --

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 1172.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULENCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39893E+01	0.10853E+01	0.50180E-07	0.24990E-09	0.45016E-01	1.02268	0.11850E-01
2	0.35112E+01	0.36321E+01	0.85843E+00	0.41340E-08	0.00000E+00	-0.15846E-01	0.99210	0.10953E-02
3	0.17005E+01	0.48542E+01	0.17725E+01	0.14160E-14	0.33720E-10	0.17019E+00	1.08751	-0.10597E-04
6	0.23382E+01	0.42736E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.92532E-01	1.04698	0.00000E+00

YNAJ	YNAW	YSJ	YSW
-0.543140E-07	0.317340E-09	0.394762E-03	0.394880E-03

Average Molec. Wt.= 28.81275  
 Turbulence factor = 1.00000  
 Re(ΕFF) = 57.533  
 Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.05563E-10  
 Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 3.92260E-07  
 Na-to-S molar flux ratio at the surface = 0.0011

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.29343E-02  
 ERROR (%) = 1.874E+02

GM = 1.26949  
 TJ (K) = 1780.95  
 PR = 0.690190  
 MOLE FRACTIONS  
 X(N2) = 0.755099  
 X(O2) = 0.065770  
 X(H2O) = 0.089565  
 X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

CASE NO: 8701 333 10. ppm Na, 1%S, 10. ppm V

V1ROP1HT

## -- INPUT PARAMETERS --

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 1172.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULENCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),.	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39893E+01	0.10853E+01	0.50180E-06	0.76960E-08	0.45016E-01	1.02268	0.11732E+00
2	0.35112E+01	0.36321E+01	0.85843E+00	0.41340E-07	0.00000E+00	-0.15846E-01	0.99210	0.10953E-01
3	0.17005E+01	0.48542E+01	0.17725E+01	0.14160E-12	0.31970E-07	0.17019E+00	1.08751	-0.10047E-01
6	0.23382E+01	0.42736E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.92532E-01	1.04698	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-06	0.716360E-07	0.394762E-03	0.394761E-03

Average Molec. Wt.= 28.81275  
 Turbulence factor = 1.00000  
 Re(EFF) = 57.533  
 Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 2.79299E-09  
 Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 3.93162E-07  
 Na-to-S molar flux ratio at the surface = 0.0099

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.18225E-01  
 ERROR (%) = 2.527E+03

GM = 1.26949  
 TJ (K) = 1780.95  
 PR = 0.690190  
 MOLE FRACTIONS  
 X(N2) = 0.755099  
 X(O2) = 0.065770  
 X(H2O) = 0.089565  
 X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

CASE NO.: 8701 131 0.1 ppm Na, 1%S, 0.1 ppm V

V1ROP1B.CFB

## - - INPUT PARAMETERS - -

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 977.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

OPTIONAL PARAMETERS  
 Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULENCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39604E+01	0.10853E+01	0.50180E-08	0.11390E-11	0.61792E-01	1.03121	0.11916E-02
2	0.35112E+01	0.36058E+01	0.85843E+00	0.41340E-09	0.00000E+00	-0.20278E-01	0.98990	0.10849E-03
3	0.17005E+01	0.48190E+01	0.17725E+01	0.14160E-16	0.68640E-10	0.22782E+00	1.11823	-0.20627E-04
6	0.23382E+01	0.42426E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.12757E+00	1.06514	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-08	0.138419E-09	0.394772E-03	0.394830E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.02262E-11

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 6.47981E-07

Na-to-S molar flux ratio at the surface = 0.0001

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.27946E-03  
 ERROR (%) = -7.157E+01

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLÉ FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

83

CASE NO.: 8701 231 1.0 ppm Na, 1%S, 0.1 ppm V

V1R0P1B.CFB

## -- INPUT PARAMETERS --

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 977.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULANCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39604E+01	0.10853E+01	0.50180E-07	0.14230E-11	0.61792E-01	1.03121	0.11918E-01
2	0.35112E+01	0.36058E+01	0.85843E+00	0.41340E-08	0.00000E+00	-0.20278E-01	0.98990	0.10849E-02
3	0.17005E+01	0.48190E+01	0.17725E+01	0.14160E-14	0.10710E-09	0.22782E+00	1.11823	-0.32183E-04
4	0.23382E+01	0.42426E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.12757E+00	1.06514	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-07	0.215623E-09	0.394772E-03	0.394800E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.06427E-10

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 6.48180E-07

Na-to-S molar flux ratio at the surface = 0.0007

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.29709E-02  
 ERROR (%) = 1.882E+02

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

CASE NO.: 8701 331 10 ppm Na, 1%S, 0.1 ppm V

V1ROP1B.CFB

## - - INPUT PARAMETERS - -

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19 TYPE = 0

TO (K) = 1806.000 PO (ATM) = 1.068000

TW (K) = 977.000 PJ (ATM) = 1.000000

Fuel/Air Mass Ratio (F) = 0.045380

## OPTIONAL PARAMETERS

Air Flow Rate (WA, G/SEC) = 2.94000

Nozzle Discharge Coef (DC) = 1.000000

Dia. Cyl. Target (DIAW, CM) = 0.31800

SHAPE = 0.0000 DIV = 0.0000

Length (hgt) Target (LW, CM) = 3.81000

## TURBULANCE

Dia. Jet Nozzle (DJ, CM) = 6.03300

TURB = 0.0000

Observed Deposition rate (WOBS, MG/HR) = 0.0045

TURIN = 0.0000 PERCENT

FSORET? = T

TURL (CM) = 0.000000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39604E+01	0.10853E+01	0.50180E-06	0.14530E-11	0.61792E-01	1.03121	0.11918E+00
2	0.35112E+01	0.36058E+01	0.85843E+00	0.41340E-07	0.46440E-17	-0.20278E-01	0.98990	0.10849E-01
3	0.17005E+01	0.48190E+01	0.17725E+01	0.14160E-12	0.11160E-09	0.22782E+00	1.11823	-0.33482E-04
5	0.23382E+01	0.42426E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.12757E+00	1.06514	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-06	0.224653E-09	0.394762E-03	0.394560E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.07115E-09

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 6.49682E-07

Na-to-S molar flux ratio at the surface = 0.0066

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.30000E-01  
 ERROR (%) = 2.789E+03

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

CASE NO: 8701 132 0.1 ppm Na, 1%S, 1.0 ppm V

V1ROP1B.CFB

## -- INPUT PARAMETERS --

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 977.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULANCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39604E+01	0.10853E+01	0.50180E-08	0.39400E-12	0.61792E-01	1.03121	0.11918E-02
2	0.35112E+01	0.36058E+01	0.85843E+00	0.41340E-09	0.00000E+00	-0.20278E-01	0.98990	0.10849E-03
3	0.17005E+01	0.48190E+01	0.17725E+01	0.14160E-16	0.82120E-11	0.22782E+00	1.11823	-0.24677E-05
6	0.23382E+01	0.42426E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.12757E+00	1.06514	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-08	0.168180E-10	0.394772E-03	0.394830E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.06591E-11

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 6.47981E-07

Na-to-S molar flux ratio at the surface = 0.0001

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.29778E-03  
 ERROR (%) = -7.116E+01

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

CASE NO: 8701 232 1.0 ppm Na, 1%S, 1.0 ppm V

V1ROP1B.CFB

## -- INPUT PARAMETERS --

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 977.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULENCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.000000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39604E+01	0.10853E+01	0.50180E-07	0.11460E-11	0.61792E-01	1.03121	0.11918E-01
2	0.35112E+01	0.36058E+01	0.85843E+00	0.41340E-08	0.00000E+00	-0.20278E-01	0.98990	0.10849E-02
3	0.17005E+01	0.48190E+01	0.17725E+01	0.14160E-14	0.69430E-10	0.22782E+00	1.11823	-0.20863E-04
5	0.23382E+01	0.42426E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.12757E+00	1.06514	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-07	0.140006E-09	0.394772E-03	0.394800E-03

Average Molec. Wt.= 28.81275  
 Turbulence factor = 1.00000  
 Re(EFF) = 57.533  
 Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.06696E-10  
 Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 6.48180E-07  
 Na-to-S molar flux ratio at the surface = 0.0007

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.29822E-02  
 ERROR (%) = 1.885E+02

GM = 1.26949  
 TJ (K) = 1780.95  
 PR = 0.690190  
 MOLE FRACTIONS  
 X(N2) = 0.755099  
 X(O2) = 0.065770  
 X(H2O) = 0.089565  
 X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

CASE NO. 8701 332 10. ppm Na, 1%S, 1.0 ppm V

V1ROP1B.CFB

## - - INPUT PARAMETERS - -

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 977.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULANCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.000000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
0.27773E+01	0.39604E+01	0.10853E+01	0.50180E-06	0.14240E-11	0.61792E-01	1.03121	0.11918E+00
0.35112E+01	0.36058E+01	0.85843E+00	0.41340E-07	0.45500E-17	-0.20278E-01	0.98990	0.10849E-01
0.17005E+01	0.48190E+01	0.17725E+01	0.14160E-12	0.10710E-09	0.22782E+00	1.11823	-0.32130E-04
0.23382E+01	0.42426E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.12757E+00	1.06514	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-06	0.215624E-09	0.394762E-03	0.394560E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.07118E-09

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 6.49682E-07

Na-to-S molar flux ratio at the surface = 0.0066

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.30001E-01  
 ERROR (%) = 2.789E+03

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

CASE NO. 8701 133 0.1 ppm Na, 1%S, 10. ppm V

V1ROP1B.CFB

## - - INPUT PARAMETERS - -

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 977.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380                    OPTIONAL PARAMETERS  
 Air Flow Rate (WA, G/SEC) = 2.94000                  Nozzle Discharge Coef (DC) = 1.000000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800                SHAPE = 0.0000        DIV = 0.0000  
 Length (hgt) Target (LW, CM) = 3.81000               TURBULENCE  
 Dia. Jet Nozzle (DJ, CM) = 6.03300                  TURB = 0.0000  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045      TURIN = 0.0000 PERCENT  
 FSORET? = T                TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39604E+01	0.10853E+01	0.50180E-08	0.12060E-12	0.61792E-01	1.03121	0.11918E-02
2	0.35112E+01	0.36058E+01	0.85843E+00	0.41340E-09	0.00000E+00	-0.20278E-01	0.98990	0.10849E-03
3	0.17005E+01	0.48190E+01	0.17725E+01	0.14160E-16	0.76920E-12	0.22782E+00	1.11823	-0.23114E-06
6	0.23382E+01	0.42426E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.12757E+00	1.06514	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-08	0.165900E-11	0.394762E-03	0.394820E-03

Average Molec. Wt.= 28.81275  
 Turbulence factor = 1.00000  
 Re(EFF) = 57.533  
 Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.07134E-11  
 Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 6.47967E-07  
 Na-to-S molar flux ratio at the surface = 0.0001

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.30008E-03  
 ERROR (%) = -7.111E+01

GM = 1.26949  
 TJ (K) = 1780.95  
 PR = 0.690190  
 MOLE FRACTIONS  
 X(N2) = 0.755099  
 X(O2) = 0.065770  
 X(H2O) = 0.089565  
 X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

89

CASE NO.: 8701 233 1.0 ppm Na, 1%S, 10. ppm V

V1ROP1B.CFB

## - - INPUT PARAMETERS - -

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 977.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

## OPTIONAL PARAMETERS

Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULENCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39604E+01	0.10853E+01	0.50180E-07	0.39460E-12	0.61792E-01	1.03121	0.11918E-01
2	0.35112E+01	0.36058E+01	0.85843E+00	0.41340E-08	0.00000E+00	-0.20278E-01	0.98990	0.10849E-02
3	0.17005E+01	0.48190E+01	0.17725E+01	0.14160E-14	0.82360E-11	0.22782E+00	1.11823	-0.24744E-05
6	0.23382E+01	0.42426E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.12757E+00	1.06514	0.00000E+00

YNAJ            YNAW            YSJ            YSW  
 0.543140E-07    0.168666E-10    0.394762E-03    0.394820E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.07135E-10

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 6.47967E-07

Na-to-S molar flux ratio at the surface = 0.0007

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.30008E-02  
 ERROR (%) = 1.889E+02

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

## CFBL THEORY FOR SODIUM SULFATE DEPOSITION RATE

CASE NO: 8701 333 10. ppm Na, 1%S, 10. ppm V

V1R0P1B.CFB

## - - INPUT PARAMETERS - -

(ALL GAS PROPERTIES PERTAIN TO TJ,PJ)

RUN = 19            TYPE = 0  
 TO (K) = 1806.000        PO (ATM) = 1.068000  
 TW (K) = 977.000        PJ (ATM) = 1.000000  
 Fuel/Air Mass Ratio (F) = 0.045380  
 Air Flow Rate (WA, G/SEC) = 2.94000  
 Dia. Cyl. Target (DIAW, CM) = 0.31800  
 Length (hgt) Target (LW, CM) = 3.81000  
 Dia. Jet Nozzle (DJ, CM) = 6.03300  
 Observed Deposition rate (WOBS, MG/HR) = 0.0045  
 FSORET? = T

OPTIONAL PARAMETERS  
 Nozzle Discharge Coef (DC) = 1.000000  
 SHAPE = 0.0000        DIV = 0.0000  
 TURBULENCE  
 TURB = 0.0000  
 TURIN = 0.0000 PERCENT  
 TURL (CM) = 0.00000

I=1=NAOH , I=2=NA , I=3=NA2SO4 , I=6=NACL

I	D(I)	NU(I)	SC(I)	X(I),	J X(I),W	TAU(I)	F(SORET),I	M(I)
1	0.27773E+01	0.39604E+01	0.10853E+01	0.50180E-06	0.11470E-11	0.61792E-01	1.03121	0.11918E+00
2	0.35112E+01	0.36058E+01	0.85843E+00	0.41340E-07	0.00000E+00	-0.20278E-01	0.98990	0.10849E-01
3	0.17005E+01	0.48190E+01	0.17725E+01	0.14160E-12	0.69510E-10	0.22782E+00	1.11823	-0.20834E-04
5	0.23382E+01	0.42426E+01	0.12891E+01	0.00000E+00	0.00000E+00	0.12757E+00	1.06514	0.00000E+00

YNAJ	YNAW	YSJ	YSW
0.543140E-06	0.140167E-09	0.394762E-03	0.394620E-03

Average Molec. Wt.= 28.81275

Turbulence factor = 1.00000

Re(EFF) = 57.533

Total Na mass flux to surface (SUM, G/CM\*\*2/SEC) = 3.07145E-09

Total S mass flux to surface (SMS, G/CM\*\*2/SEC) = 6.49285E-07

Na-to-S molar flux ratio at the surface = 0.0066

PREDICTED NA2SO4 DEPOSITION RATE (MG/HR) = 1.30012E-01  
 ERROR (%) = 2.789E+03

GM = 1.26949

TJ (K) = 1780.95

PR = 0.690190

## MOLE FRACTIONS

X(N2) = 0.755099

X(O2) = 0.065770

X(H2O) = 0.089565

X(CO2) = 0.089565

RHOJ(G/CM**3)	UJ(CM/S)	ETAMIX(POISE)	LAMIX(CAL/CM/K/S)	CMIX(CAL/G/S)
0.197159E-03	0.545317E+03	0.594261E-03	0.279215E-03	0.324288E+00

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<input type="checkbox"/> Document describes a computer program; SF-185, FIPS Software Summary, is attached.				
11. ABSTRACT (A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey, mention it here)				
<p>An integrated equilibrium kinetic model is described for treating the chemical solution component of corrosion of (Co,Cr)-based superalloys by the (Na, S, V)-molten salts originating from impurities present in hydrocarbon fuels. Gas phase chemistry and gas phase/condensed phase precipitate interactions are modeled using the NASA-Lewis multicomponent free energy minimization program (CEC). Salt deposition rates are calculated with the aid of a chemical frozen boundary layer (CFBL) program. Solubilities of superalloy components (Co and Cr) are modeled from phase equilibrium data, and rate of solution is described by assuming a very thin steady state oxide film, with formation and dissolution occurring according to a parabolic rate law. A range of steady state corrosion rates can be predicted using this approach which are in general agreement with the range of reported test rig results. Further model development would benefit from additional experimental phase equilibrium data on the system Na<sub>2</sub>O-CoO-Cr<sub>2</sub>O<sub>3</sub>-SO<sub>3</sub>-V<sub>2</sub>O<sub>5</sub>.</p>				
12. KEY WORDS (Six to twelve entries; alphabetical order; capitalize only proper names; and separate key words by semicolons) chromium; cobalt; high temperature solubility; hot corrosion; molten salts; sodium; sulfate; sulfur; superalloys, vanadate				
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